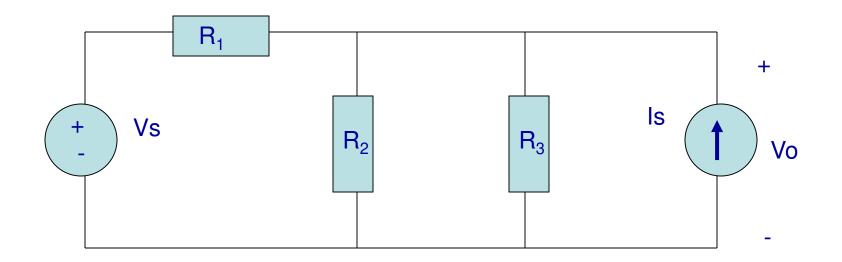
### Kirchoff's Laws

Chapter 3

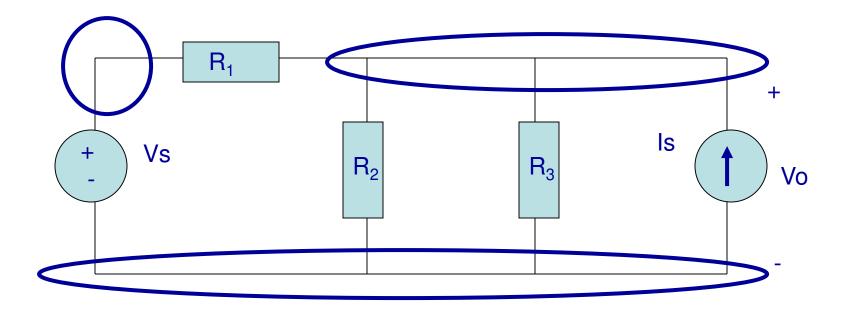
# **Circuit Definitions**

- Node any point where 2 or more circuit elements are connected together
  - Wires usually have negligible resistance
  - Each node has one voltage (w.r.t. ground)
- Branch a circuit element between two nodes
- Loop a collection of branches that form a closed path returning to the same node without going through any other nodes or branches twice

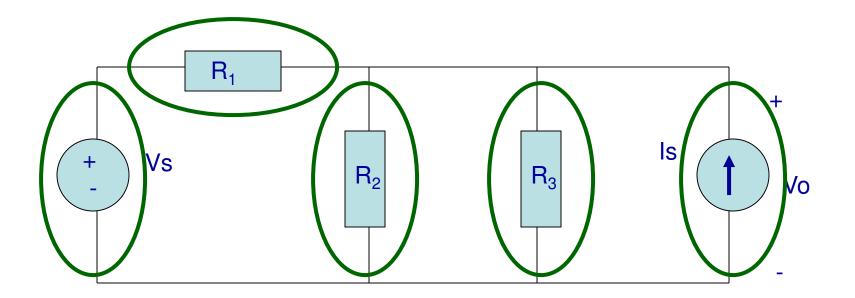
• How many nodes, branches & loops?



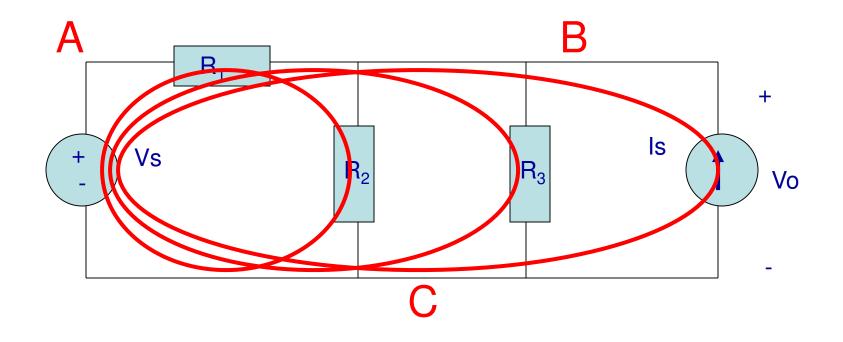
• Three nodes



• 5 Branches



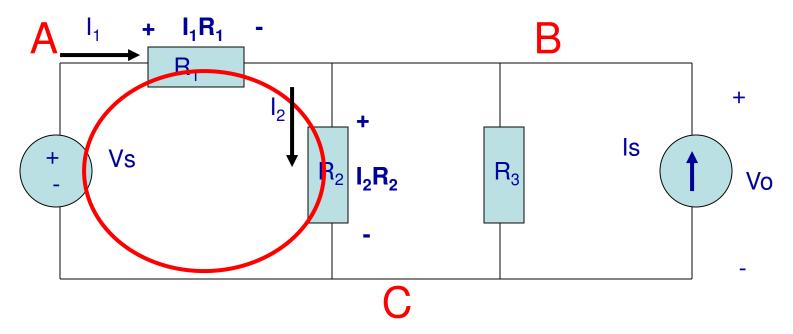
• Three Loops, if starting at node A



# Kirchoff's Voltage Law (KVL)

- The algebraic sum of voltages around each loop is zero
  - Beginning with one node, add voltages across each branch in the loop (if you encounter a + sign first) and subtract voltages (if you encounter a – sign first)
- $\Sigma$  voltage drops  $\Sigma$  voltage rises = 0
- Or  $\Sigma$  voltage drops =  $\Sigma$  voltage rises

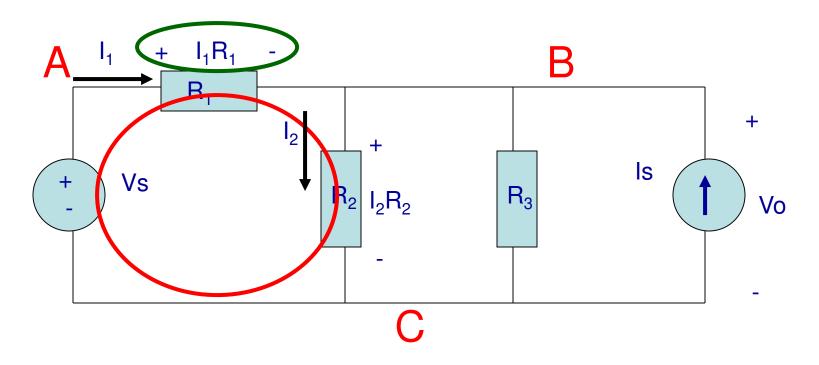
Kirchoff's Voltage Law around 1<sup>st</sup> Loop



Assign current variables and directions

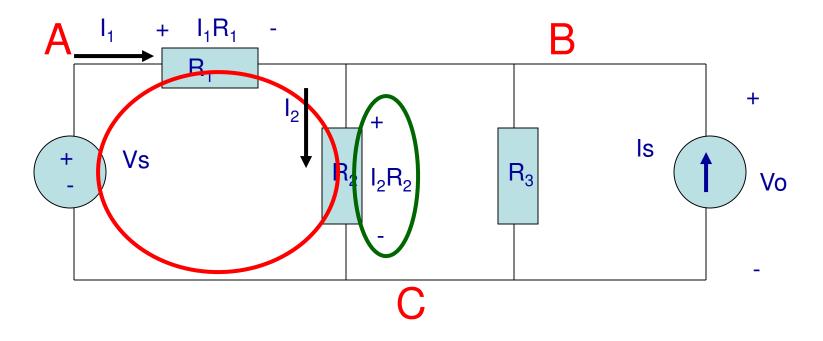
Use Ohm's law to assign voltages and polarities consistent with passive devices (current enters at the + side)

Kirchoff's Voltage Law around 1<sup>st</sup> Loop



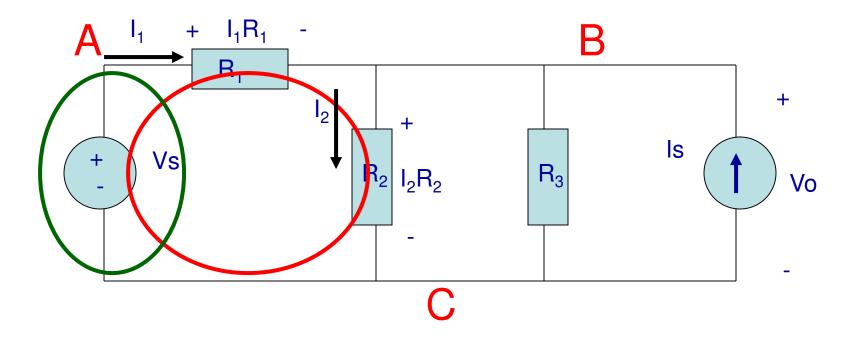
Starting at node A, add the 1<sup>st</sup> voltage drop:  $+ I_1 R_1$ 

Kirchoff's Voltage Law around 1<sup>st</sup> Loop



Add the voltage drop from B to C through  $R_2$ : +  $I_1R_1$  +  $I_2R_2$ 

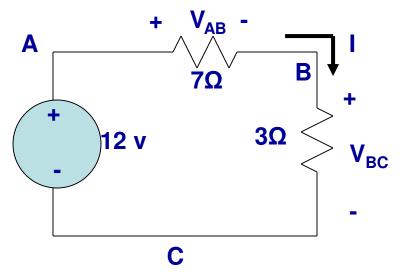
Kirchoff's Voltage Law around 1<sup>st</sup> Loop



Subtract the voltage rise from C to A through Vs:  $+I_1R_1 + I_2R_2 - Vs = 0$ Notice that the sign of each term matches the polarity encountered 1st

# **Circuit Analysis**

 When given a circuit with sources and resistors having fixed values, you can use Kirchoff's two laws and Ohm's law to determine all branch voltages and currents

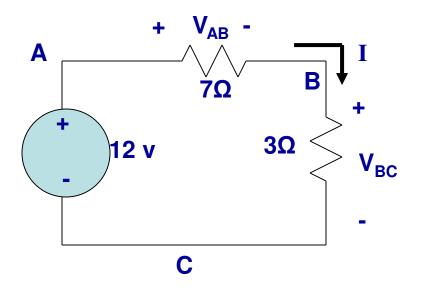


# **Circuit Analysis**

- By Ohm's law:  $V_{AB}$  =  $I{\cdot}7\Omega$  and  $V_{BC}$  =  $I{\cdot}3\Omega$
- By KVL:  $V_{AB} + V_{BC} 12 v = 0$
- Substituting:  $I \cdot 7\Omega + I \cdot 3\Omega 12 v = 0$
- Solving: I = 1.2 A A  $+ V_{AB}$   $7\Omega$  B  $+ V_{BC}$  - 12 v  $3\Omega$   $V_{BC}$ - C

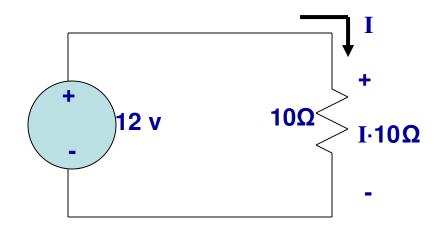
## **Circuit Analysis**

- Since  $V_{AB} = I \cdot 7\Omega$  and  $V_{BC} = I \cdot 3\Omega$
- And I = 1.2 A
- So  $V_{\text{AB}}$  = 8.4~v and  $V_{\text{BC}}$  = 3.6~v



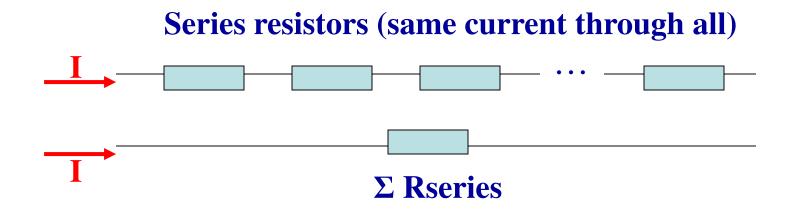
### **Series Resistors**

- KVL:  $+I \cdot 10\Omega 12 v = 0$ , So I = 1.2 A
- From the viewpoint of the source, the 7 and 3 ohm resistors in series are equivalent to the 10 ohms



### Series Resistors

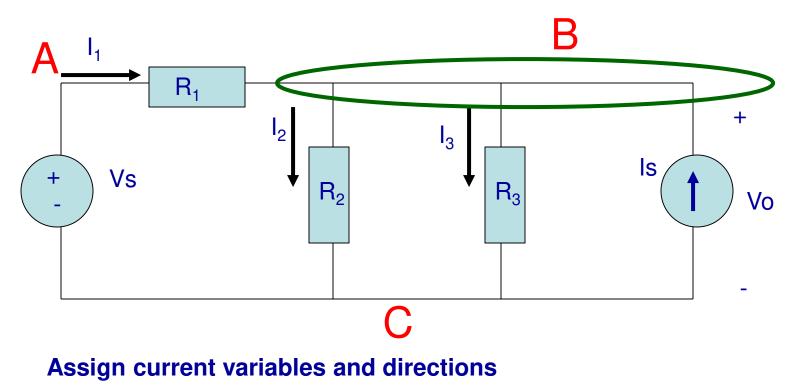
• To the rest of the circuit, series resistors can be replaced by an equivalent resistance equal to the sum of all resistors



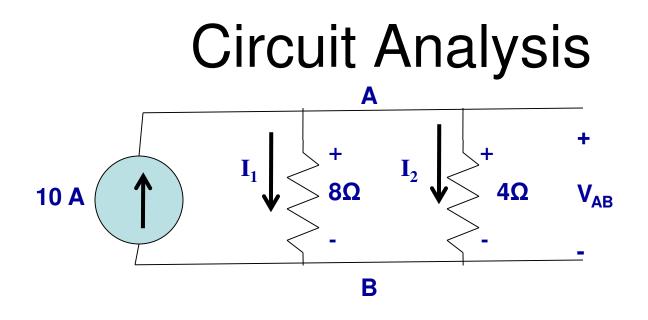
# Kirchoff's Current Law (KCL)

- The algebraic sum of currents entering a node is zero
  - Add each branch current entering the node and subtract each branch current leaving the node
- $\Sigma$  currents in  $\Sigma$  currents out = 0
- Or  $\Sigma$  currents in =  $\Sigma$  currents out

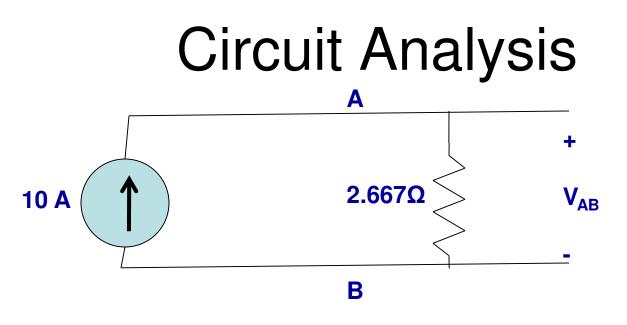
Kirchoff's Current Law at B



Add currents in, subtract currents out:  $I_1 - I_2 - I_3 + I_3 = 0$ 



By KVL:  $-I_1 \cdot 8\Omega + I_2 \cdot 4\Omega = 0$ Solving:  $I_2 = 2 \cdot I_1$ By KCL:  $10A = I_1 + I_2$ Substituting:  $10A = I_1 + 2 \cdot I_1 = 3 \cdot I_1$ So  $I_1 = 3.33$  A and  $I_2 = 6.67$  A And  $V_{AB} = 26.33$  volts



By Ohm's Law:  $V_{AB} = 10 \text{ A} \cdot 2.667 \Omega$ So  $V_{AB} = 26.67$  volts

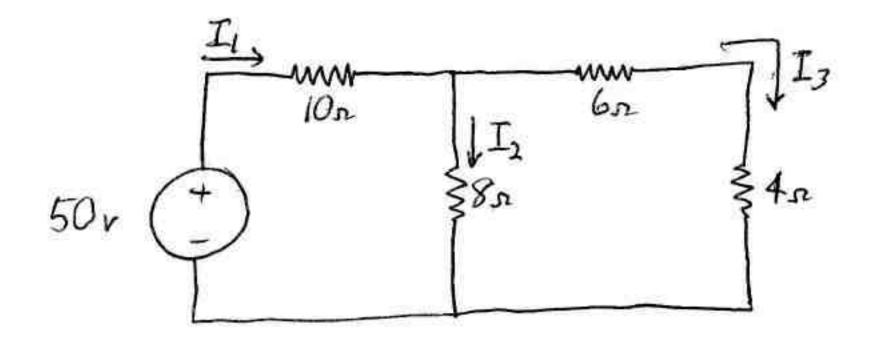
Replacing two parallel resistors (8 and 4  $\Omega$ ) by one equivalent one produces the same result from the viewpoint of the rest of the circuit.

### Parallel Resistors

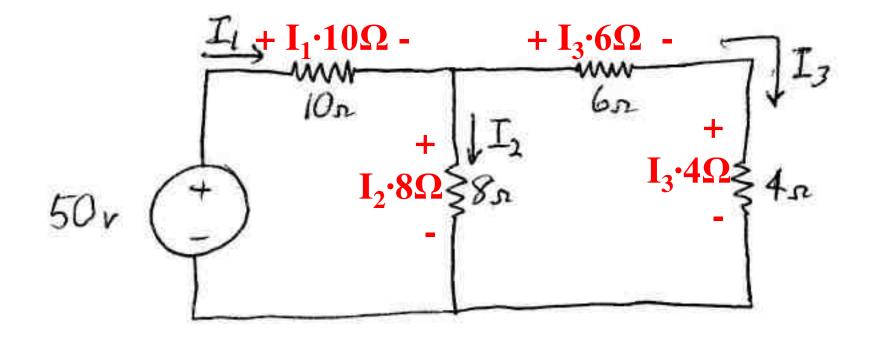
 The equivalent resistance for any number of resistors in parallel (i.e. they have the same voltage across each resistor):

Req = 
$$\frac{1}{1/R_1 + 1/R_2 + \dots + 1/R_N}$$

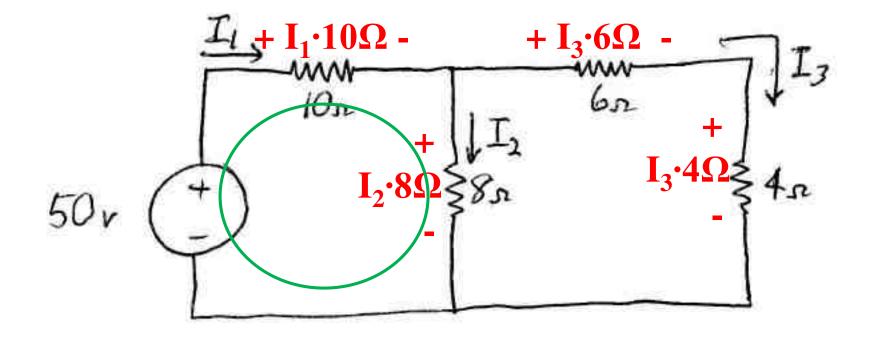
• For two parallel resistors:  $Req = R_1 \cdot R_2 / (R_1 + R_2)$ 



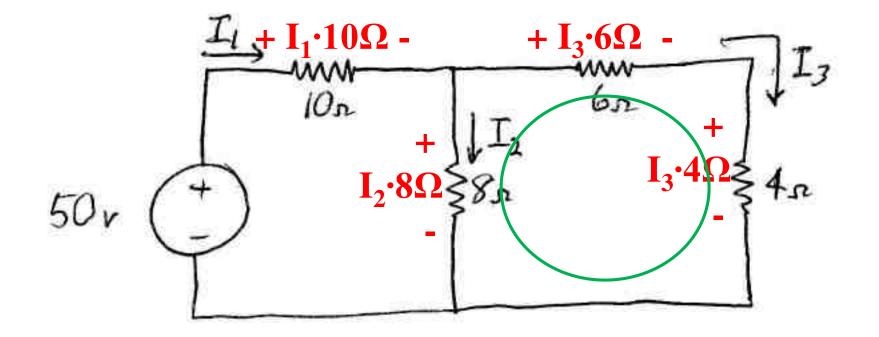
Solve for the currents through each resistor And the voltages across each resistor



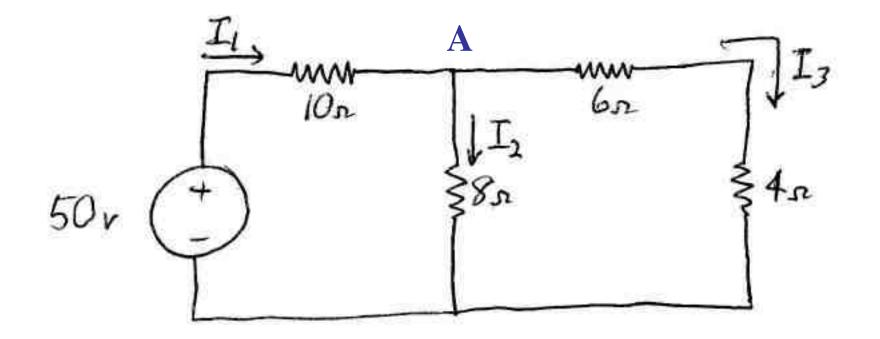
Using Ohm's law, add polarities and expressions for each resistor voltage



Write 1<sup>st</sup> Kirchoff's voltage law equation -50 v +  $I_1$ ·10 $\Omega$  +  $I_2$ ·8 $\Omega$  = 0



Write 2<sup>nd</sup> Kirchoff's voltage law equation  $-I_2 \cdot 8\Omega + I_3 \cdot 6\Omega + I_3 \cdot 4\Omega = 0$ or  $I_2 = I_3 \cdot (6+4)/8 = 1.25 \cdot I_3$ 



Write Kirchoff's current law equation at A + $I_1 - I_2 - I_3 = 0$ 

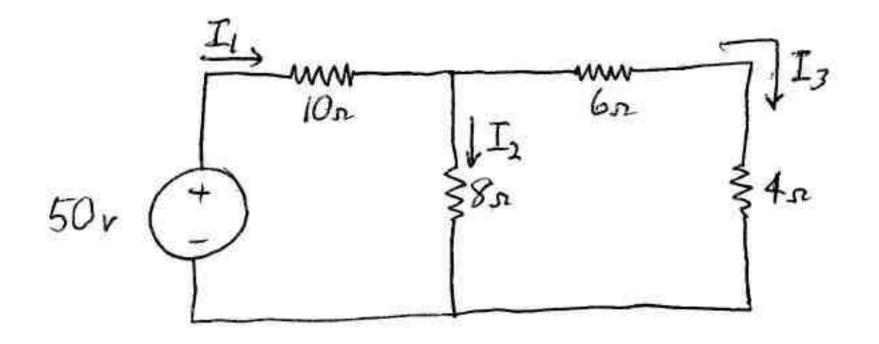
- We now have 3 equations in 3 unknowns, so we can solve for the currents through each resistor, that are used to find the voltage across each resistor
- Since  $I_1 I_2 I_3 = 0$ ,  $I_1 = I_2 + I_3$
- Substituting into the 1st KVL equation  $-50 v + (I_2 + I_3) \cdot 10\Omega + I_2 \cdot 8\Omega = 0$ or  $I_2 \cdot 18 \Omega + I_3 \cdot 10 \Omega = 50$  volts

- But from the 2<sup>nd</sup> KVL equation,  $I_2 = 1.25 \cdot I_3$
- Substituting into 1<sup>st</sup> KVL equation:  $(1.25 \cdot I_3) \cdot 18 \Omega + I_3 \cdot 10 \Omega = 50$  volts Or:  $I_3 \cdot 22.5 \Omega + I_3 \cdot 10 \Omega = 50$  volts

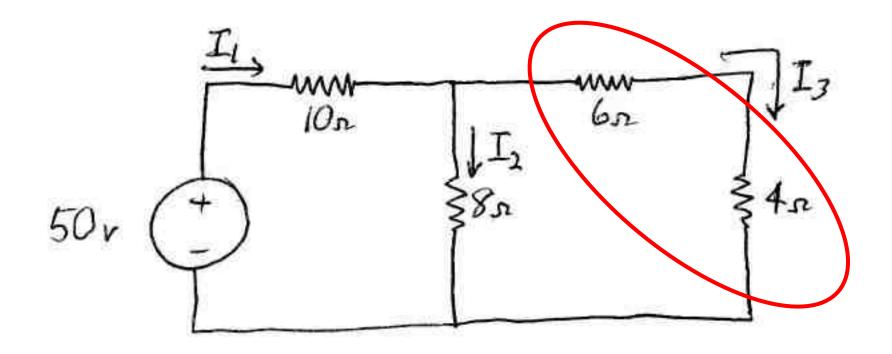
Or: 
$$I_3 \cdot 32.5 \Omega = 50$$
 volts

- Or:  $I_3 = 50 \text{ volts}/32.5 \Omega$
- Or:  $I_3 = 1.538$  amps

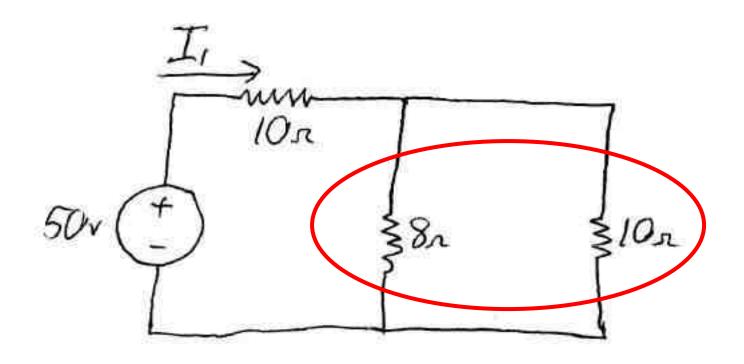
- Since  $I_3 = 1.538$  amps  $I_2 = 1.25 \cdot I_3 = 1.923$  amps
- Since  $I_1 = I_2 + I_{3,}$   $I_1 = 3.461$  amps
- The voltages across the resistors:  $I_1 \cdot 10\Omega = 34.61$  volts  $I_2 \cdot 8\Omega = 15.38$  volts  $I_3 \cdot 6\Omega = 9.23$  volts
  - $I_3 \cdot 4\Omega = 6.15$  volts



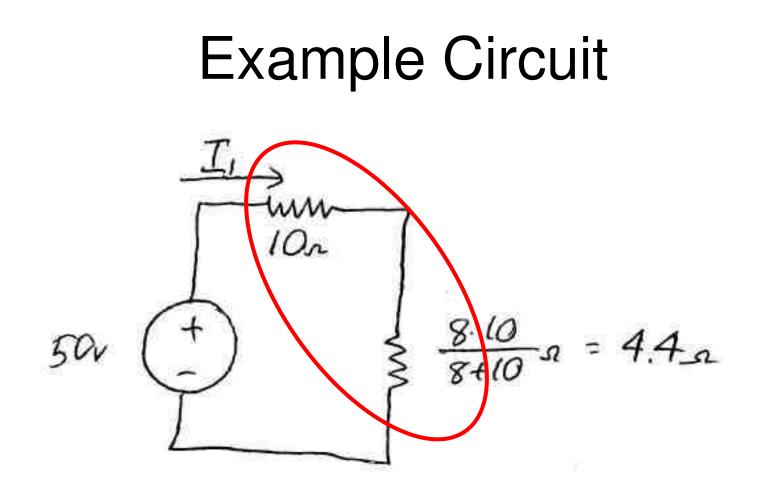
Solve for the currents through each resistor And the voltages across each resistor using Series and parallel simplification.



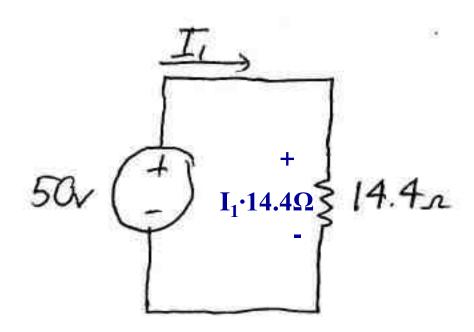
The 6 and 4 ohm resistors are in series, so are combined into  $6+4 = 10\Omega$ 



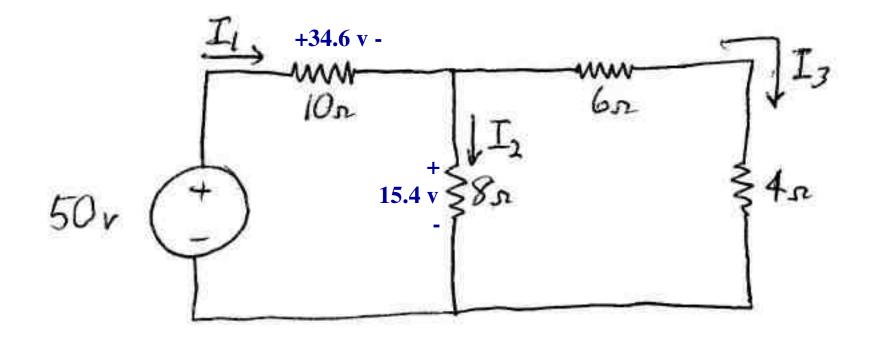
The 8 and 10 ohm resistors are in parallel, so are combined into  $8\cdot10/(8+10) = 14.4 \Omega$ 



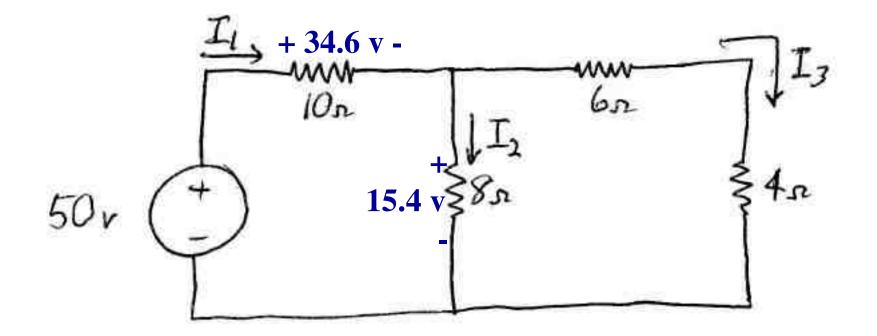
The 10 and 4.4 ohm resistors are in series, so are combined into  $10+4 = 14.4\Omega$ 



Writing KVL,  $I_1 \cdot 14.4\Omega - 50 v = 0$ Or  $I_1 = 50 v / 14.4\Omega = 3.46 A$ 



If  $I_1 = 3.46$  A, then  $I_1 \cdot 10 \Omega = 34.6$  v So the voltage across the 8  $\Omega = 15.4$  v



If  $I_2 \cdot 8 \Omega = 15.4 \text{ v}$ , then  $I_2 = 15.4/8 = 1.93 \text{ A}$ By KCL,  $I_1 \cdot I_2 \cdot I_3 = 0$ , so  $I_3 = I_1 - I_2 = 1.53 \text{ A}$ 

# **Objectives**

•At the end of this topic, you should be able to:

- apply the superposition theorem for circuit analysis
- apply Thevenin's theorem to simplify the circuit for analysis
- apply Norton's theorem to simplify the circuit for analysis
- understand maximum power transfer and perform circuit conversion

### **Network Theorems**

# **Objectives**

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### **Network Theorems**

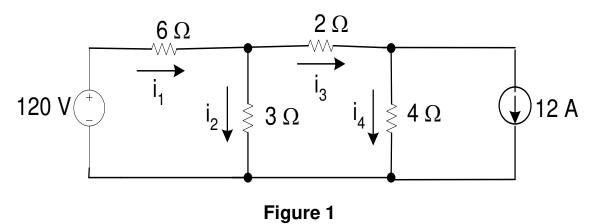
# **Objectives**

•At the end of this topic, you should be able to:

- apply the superposition theorem for circuit analysis
- apply Thevenin's theorem to simplify the circuit for analysis
- apply Norton's theorem to simplify the circuit for analysis
- understand maximum power transfer and perform circuit conversion

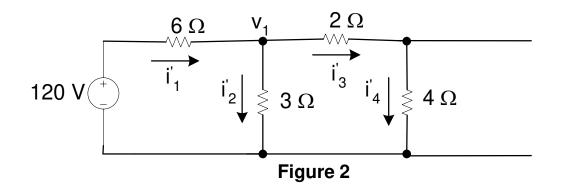
# **Superposition Theorem**

• The Superposition theorem states that if a linear system is driven by more than one independent power source, the total response is the sum of the individual responses. The following example will show the step of finding branches current using superpostion theorem Refer to the Figure 1, determine the branches current using superposition theorem.



#### Solution

• The application of the superposition theorem is shown in Figure 1, where it is used to calculate the branch current. We begin by calculating the branch current caused by the voltage source of 120 V. By substituting the ideal current with open circuit, we deactivate the current source, as shown in Figure 2.

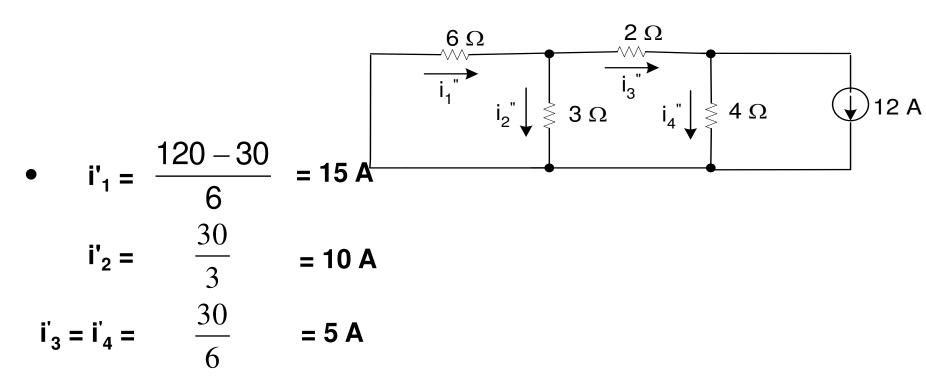


• To calculate the branch current, the node voltage across the  $3\Omega$  resistor must be known. Therefore

$$\frac{v_1 - 120}{6} + \frac{v_1}{3} + \frac{v_1}{2 + 4} = 0$$

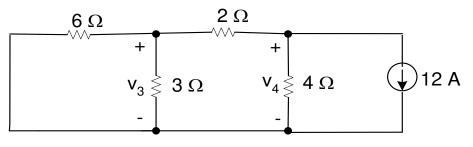
where  $v_1 = 30 V$ 

The equations for the current in each branch,



#### In order to calculate the current cause by the current source, we deactivate the ideal voltage source with a short circuit, as shown

• To determine the branch current, solve the node voltages across the  $3\Omega$  dan  $4\Omega$  resistors as shown in Figure 4



$$\frac{v_3}{3} + \frac{v_3}{6} + \frac{v_3 - v_4}{2} = 0$$

$$\frac{v_4 - v_3}{2} + \frac{v_4}{4} + 12 = 0$$

• The two node voltages are

# By solving these equations, we obtain v<sub>3</sub> = -12 V v<sub>4</sub> = -24 V

Now we can find the branches current,

$$i_{1}'' = \frac{-v_{3}}{6} = \frac{12}{6} = 2A$$

$$i_{2}'' = \frac{v_{3}}{3} = \frac{-12}{3} = -4A$$

$$i_{3}'' = \frac{v_{3} - v_{4}}{2} = \frac{-12 + 24}{2} = 6A$$

$$i_{4}'' = \frac{v_{4}}{4} = \frac{-24}{4} = -6A$$

# To find the actual current of the circuit, add the currents due to both the current and voltage source,

$$i_{1} = i'_{1} + i''_{1} = 15 + 2 = 17 A$$

$$i_{2} = i'_{2} + i''_{2} = 10 - 4 = 6 A$$

$$i_{3} = i'_{3} + i''_{3} = 5 + 6 = 11 A$$

$$i_{4} = i'_{4} + i''_{4} = 5 - 6 = -1 A$$

#### **Thevenin and Norton Equivalent Circuits**

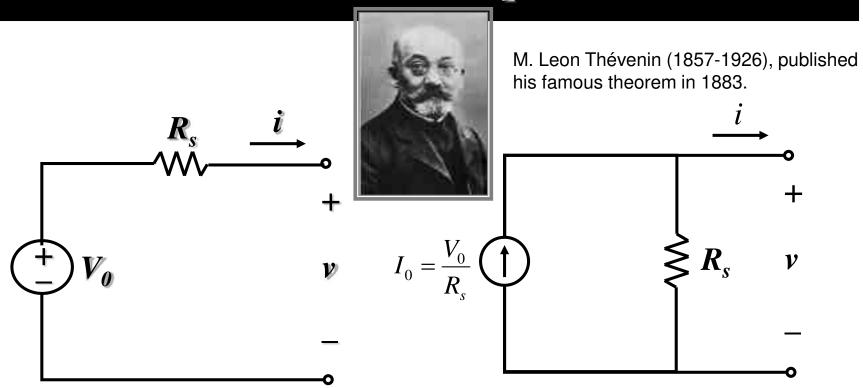


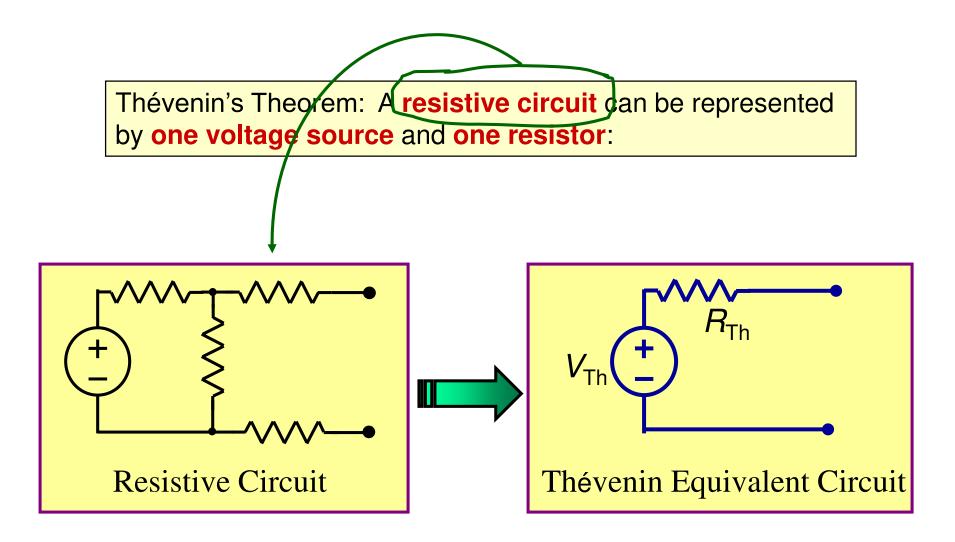
Fig.2.17 (a) Thevenin equivalent circuit ; (b) Norton equivalent circuit

$$v = V_0 - R_s i \qquad \qquad i = I_0 - \frac{v}{R_s}$$

The equivalence of these two circuits is a special case of the *Thevenin and Norton Theorem* 

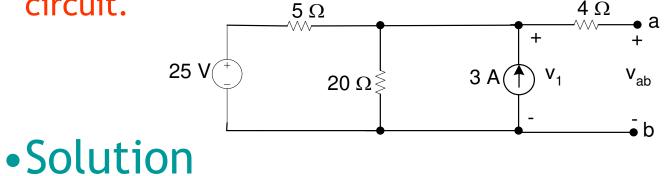
#### **Thevenin & Norton Equivalent Circuits**

- Thevenin's Theorem states that it is possible to simplify any linear circuit, no matter how complex, to an equivalent circuit with just a single voltage source and series resistance connected to a load.
   A series combination of Thevenin equivalent voltage source V<sub>0</sub> and Thevenin equivalent resistance R<sub>s</sub>
- Norton's Theorem states that it is possible to simplify any linear circuit, no matter how complex, to an equivalent circuit with just a single current source and parallel resistance connected to a load. Norton form:
  - A parallel combination of Norton equivalent current source  $I_0$  and Norton equivalent resistance  $R_s$



• Example

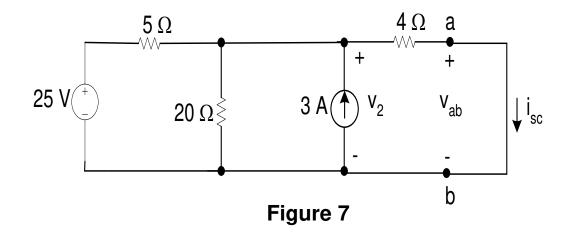
Refer to the Figure 6, find the Thevenin equivalent circuit.  $5\Omega$   $4\Omega$ 



- In order to find the Thevenin equivalent circuit for the circuit shown in Figure 6, calculate the open circuit voltage, vab. Note that when the a, b terminals are open, there is no current flow to  $4\Omega$  resistor. Therefore, the voltage vab is the same as the voltage across the 3A current source, labeled v<sub>1</sub>.
- To find the voltage  $v_1$ , solve the equations for the singular node voltage. By choosing the bottom right node as the reference node,

$$\frac{v_1 - 25}{5} + \frac{v_1}{20} - 3 = 0$$

- By solving the equation, v1 = 32 V. Therefore, the Thevenin voltage Vth for the circuit is 32 V.
- The next step is to short circuit the terminals and find the short circuit current for the circuit shown in Figure 7. Note that the current is in the same direction as the falling voltage at the terminal.



Current  $i_{sc}$  can be found if  $v_2$  is known. By using the bottom right node as the reference node, the equation for  $v_2$  becomes

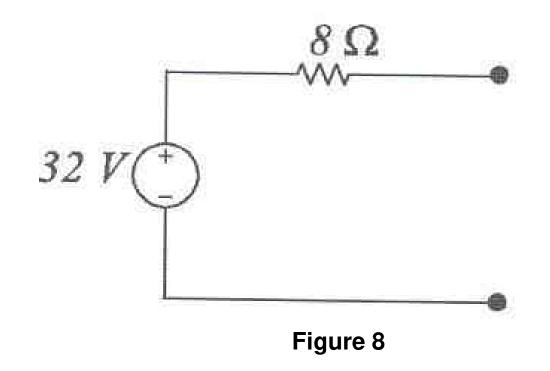
By solving the above equation,  $v_2 = 16$  V. Therefore, the short circuit current  $i_{sc}$  is

$$\frac{v_2 - 25}{5} + \frac{v_2}{20} - 3 + \frac{v_2}{4} = 0$$
$$i_{sc} = \frac{16}{4} = 4A$$

The Thevenin resistance  $R_{\rm Th}$  is

$$R_{Th} = \frac{V_{Th}}{i_{so}} = \frac{32}{4} = 8\Omega$$

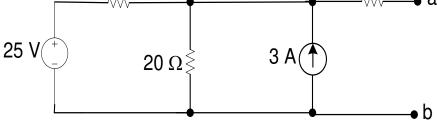
Figure 8 shows the Thevenin equivalent circuit for the Figure 6.



## Norton's Theorem

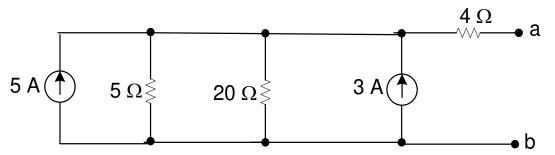
• The Norton equivalent circuit contains an independent current source which is parallel to the Norton equivalent resistance. It can be derived from the Thevenin equivalent circuit by using source transformation. Therefore, the Norton current is equivalent to the short circuit current at the terminal being studied, and Norton resistance is equivalent to Thevenin resistance.

### • Example 3 Derive the Thevenin and Norton equivalent circuits of Figure 6. $5\Omega - 4\Omega$

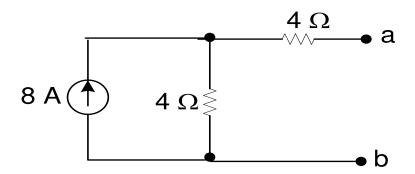


#### • Solution

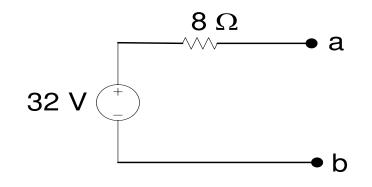
Step 1: Source transformation (The 25V voltage source is converted to a 5 A current source.)



Step 2: Combination of parallel source and parallel resistance



Step 3: Source transformation (combined serial resistance to produce the Thevenin equivalent circuit.)



Step 4: Source transformation (To produce the Norton equivalent circuit. The current source is 4A  $(I = V/R = 32 V/8 \Omega)$ )

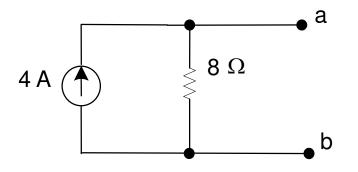
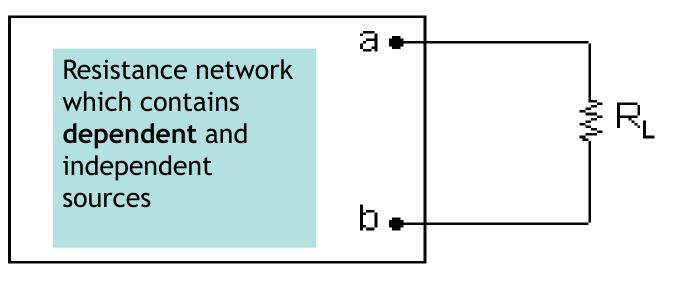


Figure 9 Steps in deriving Thevenin and Norton equivalent circuits.

## Maximum Power Transfer

• Maximum power transfer can be illustrated by Figure 10. Assume that a resistance network contains independent and dependent sources, and terminals a and b to which the resistance RL is connected. Then determine the value of RL that allows the delivery of maximum power to the load resistor.





• Maximum power transfer happens when the load resistance  $R_L$  is equal to the Thevenin equivalent resistance,  $R_{Th}$ . To find the maximum power delivered to  $R_L$ ,

$$p_{max} = \frac{V_{Th}^2 R_L}{(2R_L)^2} = \frac{V_{Th}^2}{4R_L}$$

# **Circuit Transformation**

 The configuration of circuit connection can be changed to make the calculation easier. There are TWO type of transformations which are Delta (Δ) to star connection (Y) and vice versa.

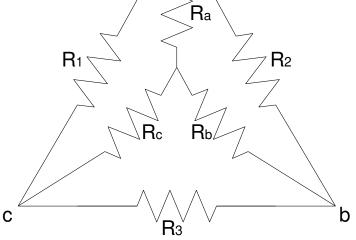


Figure 12 Delta and Star Circuit Connection

#### • Delta ( $\Delta$ ) to star (Y) transformation:

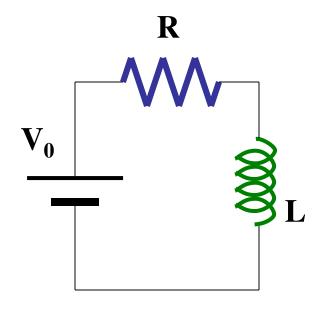
$$R_{a} = \frac{R_{1}R_{2}}{R_{1} + R_{2} + R_{3}}$$
$$R_{b} = \frac{R_{2}R_{3}}{R_{1} + R_{2} + R_{3}}$$
$$R_{c} = \frac{R_{1}R_{3}}{R_{1} + R_{2} + R_{3}}$$

#### • Star (Y) to Delta ( $\Delta$ ) transformation:

$$R_{1} = \frac{R_{a}R_{b} + R_{b}R_{c} + R_{c}R_{a}}{R_{b}}$$
$$R_{2} = \frac{R_{a}R_{b} + R_{b}R_{c} + R_{c}R_{a}}{R_{c}}$$
$$R_{3} = \frac{R_{a}R_{b} + R_{b}R_{c} + R_{c}R_{a}}{R_{a}}$$

# • Thank You

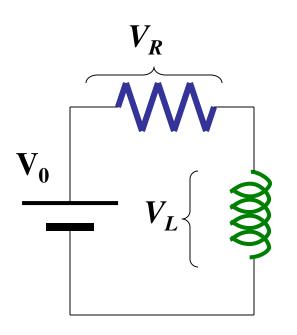
#### Inductors - how do they work?



$$V_L = L \frac{dI}{dt}$$

Start with no current in the circuit. When the battery is connected, the inductor is resistant to the flow of current. Gradually the current increases to the fixed value  $V_0/R$ , meaning that the voltage across the inductor goes to zero. In reality the inductor has a finite resistance since it is a long wire so it will then be more like a pair of series resistances.

#### Inductors - time constant L/R



Again the behavior of an inductor is seen by analysis with Kirchoff's laws. Suppose we start with no current.

$$V_0 = V_R + V_L = IR + L\frac{dI}{dt}$$

then 
$$I = \frac{V_0}{R} \left[ 1 - \exp\left[-\frac{Rt}{L}\right] \right]$$
 and  
 $V_L = V_0 \exp\left[-\frac{Rt}{L}\right] \quad V_R = V_0 \left(1 - \exp\left[-\frac{Rt}{L}\right]\right)$ 

There is a fundamental time scale set by L/R, which has units of seconds (=Henry/Ohm)

#### RLC circuits with sinusoidal sources

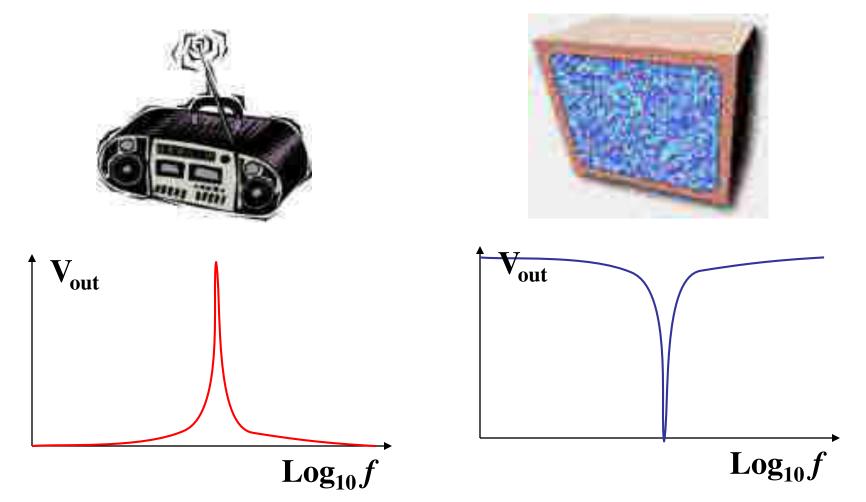
The AC analysis of circuits with inductors is also easy, with the effective resistance (impedance) of an inductor equal to  $i \mathbb{P}L$ . From a phasor point of view this means that the inductor leads the resistor by 90 degrees.

High pass and low pass filters can be made from inductors as well. However the inductors are usually bulkier and relatively expensive compared to capacitors (and more difficult to make in an integrated circuit) so are not used as commonly.

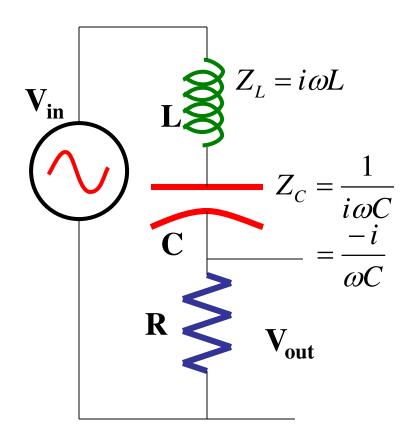
Another limitation is that they are far from ideal. The impedance is usually  $R_L + i \mathbb{P}L$ , which means that in order to find the breakpoint you use  $f = L/(2\mathbb{P}(R_L + R))$ .

#### Notch and Bandpass

A filter can also serve to select or eliminate a narrow band of frequencies. Examples are radio (select) and parental control "channel eliminator" circuits.



# Mathematical analysis of a series LRC circuit - bandpass filter



First find the total impedance of the circuit

$$Z = R + i \left( \omega L - \frac{1}{\omega C} \right)$$

Using a voltage divider

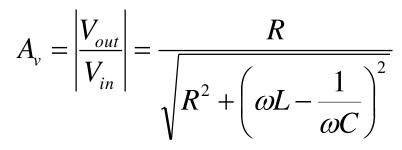
$$\frac{V_{out}}{V_{in}} = \frac{R}{R + i \left(\omega L - \frac{1}{\omega C}\right)}$$

The phase shift goes from 90° to -90°.

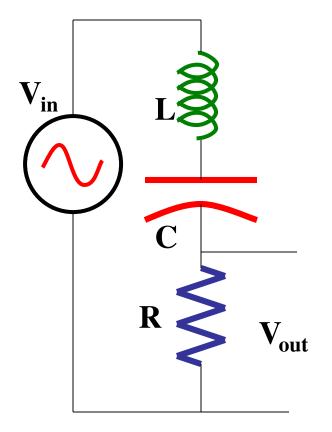
$$\phi = -\tan^{-1}\frac{R}{\left(\omega L - \frac{1}{\omega C}\right)}$$

# Mathematical analysis of a series LRC circuit - bandpass filter (2)

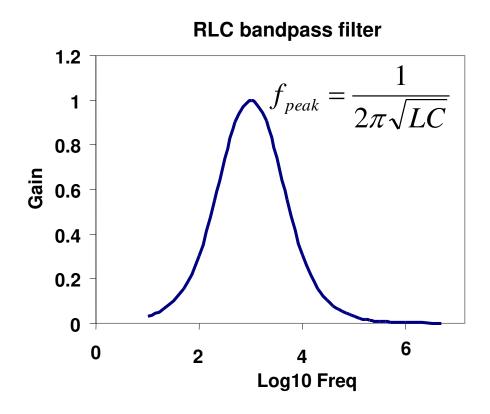
The magnitude of the gain,  $A_v$ , is



Note that for high frequencies  $\square L$  is dominant and the gain is  $R/ \square L$  or small. At low frequencies the gain is  $\square RC$ because the impedance of the capacitor is dominant. At  $\square^2 =$  1/LC the gain is one (assuming ideal components).

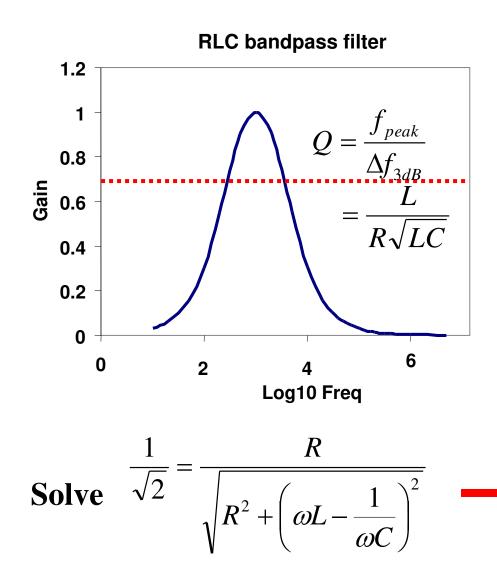


### Graphing for a series LRC circuit



Although the gain falls off at 20 dB/decade at high and low frequencies (this means that it is proportional to ?) it is more typical to plot it as shown on a semi-log graph, since this emphasizes the peak.

### Q factor for a Series LRC circuit



The quality factor or Q is defined as the energy stored divided by the energy loss/cycle. For an electronic bandpass it is the peak frequency divided by the width of the peak or bandwidth (defined by the frequencies where the gain is 3 dB lower than the maximum).R

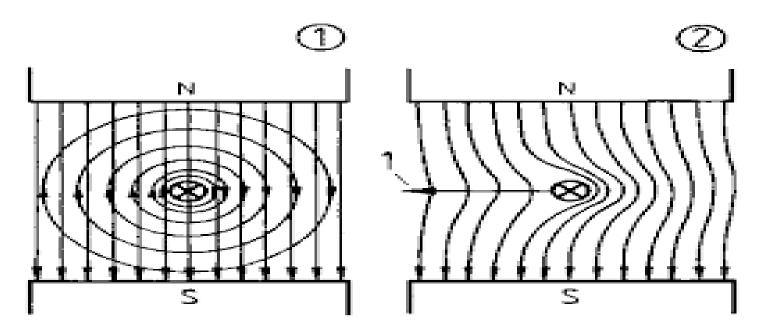
### **Course outcome**

C403.4: Identify and select various electrical machines based on their characteristics and applications

## Introduction

- The Dc machines are of two types namely DC generators and DC motors.
- A DC generators converts mechanical energy into electrical energy whereas a DC motor converts the electrical energy into mechanical energy.
- In order to understand the operating principle of a DC motor, it is necessary to understand how does a current carrying conductor experience a force, when kept in a magnetic field.

- Force on current carrying conductor:
- ➢ If a straight conductor is placed in the magnetic field produced by a permanent magnet, the current flowing through a conductor in anti clockwise direction.
- Due to the presence of two magnetic fields simultaneously, an interaction between them will take place as shown in fig.(1).



**Fig.1(a): Interaction of the fields** 

Fig.1(b):Resultant field

- ➤ As shown in fig.(1), the flux lines produced by the magnet and the conductor are in opposite direction to each other at left side and hence cancel each other. Therefore the no of flux lines at left side will reduced.
- ➤ At the right side, the individual fields are in the same direction, hence will add or strengthen each other. Therefore the no. of flux lines at right side will increase.

Magnitude of Force:

➤ The magnitude of the force experienced by the current carrying conductor placed in the magnetic field is given by,

F = BIl Newton

Where B = Flux density produced by Magnet

I = current flowing through conductor

l = Length of the conductor

#### • Direction of force:

- The direction of rotation of a motor depends on the direction of force exerted on the the armature winding and the direction of force experienced by a current carrying conductor is given by Fleming's left hand rule.
- > Statement of Fleming's left hand rule:

It states that if the first three fingers of the left hand are held mutually at right angles to each other and if index finger indicates the direction of the magnetic field, and if middle finger indicates the direction of current flowing through the conductor, then thumb indicates the direction of force exerted on the conductor. This is shown in fig (2).

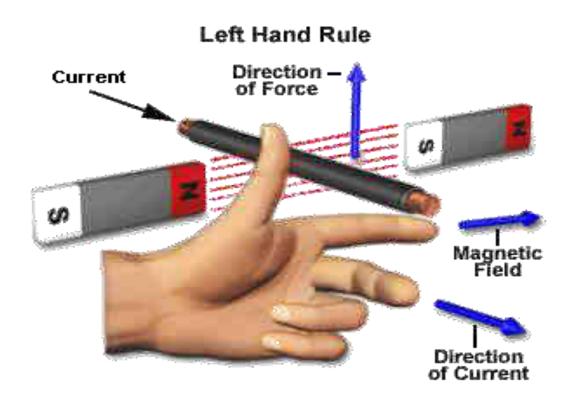


Fig.(2):Fleming's left hand rule thumb

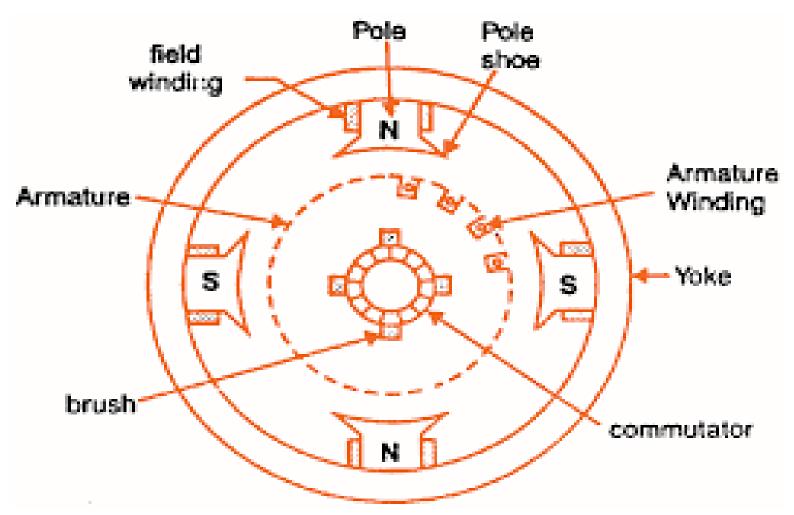
## Windings in DC Machine

- In any dc machines, there are two windings:
- 1. Field winding 2. Armature winding
- Out of these, the field winding is stationary which does not move at all and armature winding is mounted on a shaft. So it can rotate freely.
- Connection of windings for operation as motor:
- To operate the dc machine as a motor, the field winding and armature winding is connected across a dc power supply.

### **DC Motor**

- Principle of operation:
- When current carrying conductor is placed in a magnetic field, it experienced a force.
- In case of DC motor, the magnetic field us developed by the field current i.e. current flowing in field winding and armature winding plays the role of current carrying conductor
- So armature winding experienced a force and start rotating.

### **Construction of DC Motor**



**Fig.(1): construction of DC motor** 

- Important parts of DC motor:
- 1. Yoke

4. Armature

- 2. Field winding
- 3. poles 6. Brushe
- 5. Commutator, brushes & gear6. Brushes

### 1. Yoke:

- $\succ$  It acts as the outer support of a DC motor.
- $\succ$  It provides mechanical support for the poles.

#### 2. Poles:

- $\succ$  pole of a dc motor is an electromagnet.
- $\succ$  The field winding is wound over the poles.
- Poles produces magnetic flux when the filed winding is excited.

#### 3. Field winding:

- ➤ The coils wound around the pole are called field coils and they are connected in series with each other to form field winding.
- When current passing through the field winding, magnetic flux produced in the air gap between pole and armature.

#### 4. Armature:

- Armature is a cylindrical drum mounted on shaft in which number of slots are provided.
- $\succ$  Armature conductors are placed in these slots.
- Theses armature conductors are interconnected to form the armature winding.

### 5. Commutator:

- A commutator is a cylindrical drum mounted on the shaft alonwith the armature core.
- ➢ It collects the current from the armature conductors and passed it to the external load via brushes.

### 6. Brushes:

- Commutator is rotating. So it is not possible to connect the load directly to it.
- Hence current is conducted from the armature to the external load by the carbon brushes which are held against the surface of commutator by springs.

### **Back EMF**

- When the armature winding of a dc motor starts rotating in the magnetic flux produced by the field winding, it cuts the lines of magnetic flux.
- Hence according to the faraday's laws of electromagnetic induction, there will be an induced emf in the armature winding.
- As per the Lenz's law, this induced emf acts in opposite direction to the armature supply voltage. Hence this emf is called as the back emf and denoted by E<sub>b</sub>.

$$E_{b} = \frac{NP\phi Z}{60 A}$$

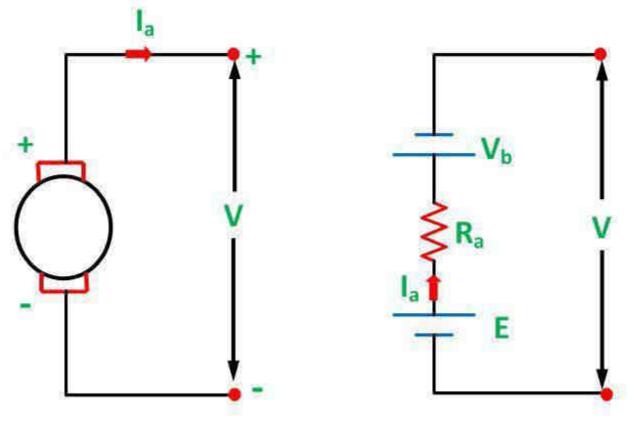
### • Significance of back emf:

- The presence of back e.m.f. makes the d.c. motor a self -regulating machine i.e., it makes the motor to draw as much armature current as is just sufficient to develop the torque required by the load.
- 1. When the motor is running on no load, small torque is required to overcome the friction and windage losses. Therefore, the armature current  $I_a$  is small and the back e.m.f. is nearly equal to the applied voltage.

2. If the motor is suddenly loaded, the first effect is to cause the armature to slow down. Therefore, the speed at which the armature conductors move through the field is reduced and hence the back e.m.f. Eb falls. The decreased back e.m.f. allows a larger current to flow through the armature and larger current means increased driving torque. Thus, the driving torque increases as the motor slows down. The motor will stop slowing down when the armature current is just sufficient to produce the increased torque required by the load.

**3**. If the load on the motor is decreased, the driving torque is momentarily in excess of the requirement so that armature is accelerated. As the armature speed increases, the back e.m.f. Eb also increases and causes the armature current Ia to decrease. The motor will stop accelerating when the armature current is just sufficient to produce the reduced torque required by the load. It follows, therefore, that back e.m.f. in a d.c. motor regulates the flow of armature current i.e., it automatically changes the armature current to meet the Load requirement.

### **Voltage Equation of a DC Motor**



**Fig.(1):Equivalent circuit of DC motor** 

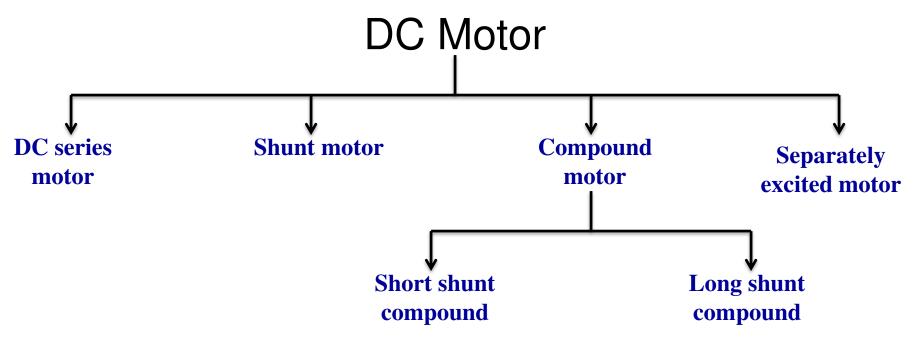
Circuit Globe

- As shown in fig.(1), the armature supply voltage V has to overcome the opposition posed by the back emf E<sub>b</sub> and some other voltage drops such as brush drop and the voltage drop across R<sub>a</sub>.
- From fig.(1), we can write that,  $V = E_b + I_a R_a + V_b$  .....(1)
- But voltage drop across brushes is negligible.

$$\therefore V = E_b + I_a R_a \qquad \dots \dots (2)$$

# **Types of DC Motors**

 Depending on the way of connecting the armature and field windings of a d.c. motors are classified as follows:



### **DC Shunt Motor**

- In DC shunt type motor, field and armature winding are connected in parallel as shown in fig.(1), and this combination is connected across a common dc power supply.
- The resistance of shunt field winding  $(R_{sh})$  is always much higher than that of armature winding  $(R_a)$ .
- This is because the number of turns for the field winding is more than that of armature winding.

• The field current  $I_{sh}$  always remains constant. Since V and  $R_{sh}$  both are constant. Hence flux produced also remains constant. Because field current is responsible for generation of flux.

 $\therefore \phi \propto I_{sh}$ 

• This is why the shunt motor is also called as the constant flux motors.

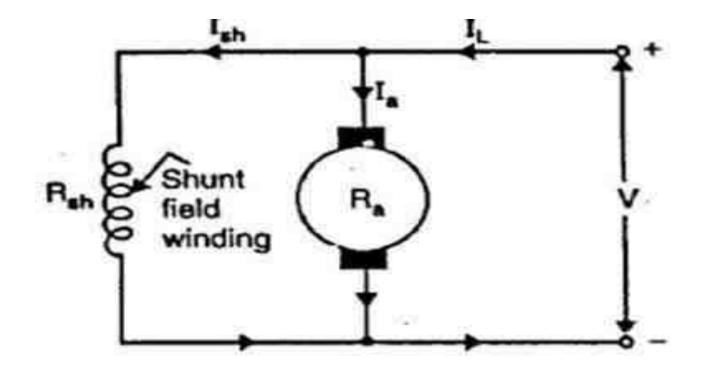
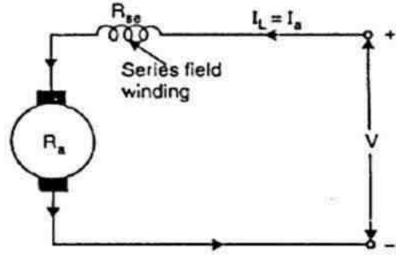


Fig.(1):DC shunt motor schematic diagram

### **DC Series Motor**

- In DC series motor, the armature and field windings are connected din series with each other as shown in fig.(1).
- The resistance of the series field winding  $(R_s)$  is much smaller as compared to that of the armature resistance  $(R_a)$ .
- The flux produced is proportional to the field current. But in series motor, the field current is same as armature current.

- The armature current  $I_a$  and hence field current Is will be dependent on the load.
- Hence in DC series motor the flux does not remains constant.



**Fig.(1):DC series motor schematic diagram** 

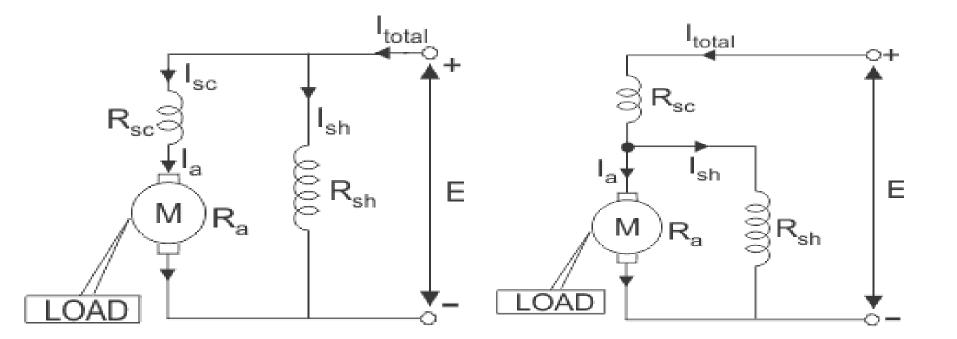
# **DC Compound Motor**

#### 1. Long Shunt Compound Motor:

• As shown in fig.(1), in long shunt dc motor, shunt field winding is connected across the series combination of the armature and series field winding.

### 2. Short Shunt Compound Motor:

- In short shunt compound motor, armature and field windings are connected in parallel with each other and this combination is connected din series with the series filed winding. This is shown in fig.(2).
- The long shunt and short shunt compound motors are further classified as cumulative and differential compound motors



**Fig.(1): Long shunt compound dc motor** 

fig.(2):Short shunt compound dc motor

# **Torque & Speed Equations**

#### • Torque equations:

- > Torque produced by a motor will always be proportional to the air gap flux  $\emptyset$  and the current flowing through the armature winding (I<sub>a</sub>).
- $\succ$  That means T  $\propto \phi I_a$
- The flux is produced by the field current hence ø will be proportional to field current. That means,

 $\phi \propto I_{\text{field}}$ 

➢ hence torque produced by a dc motor is proportional to the product of  $I_a$  and  $I_{field}$ . That means,

$$T \propto I_a I_{field}$$
 .....(1)

For various types of dc motors the expression for field current will be different. We will substitute them into eq.(1) to get the torque equations.

- 1. Torque equation of DC shunt motor:
- > For DC shunt motor Ifield = V/  $R_{sh}$  = constant
- $\succ$  Hence the flux  $\phi$  is constant.

 $\therefore T \propto I_a \qquad \dots \dots (2)$ 

- Hence in dc shunt motor, torque is proportional to only to the armature current.
- **2. Torque equation DC series motor:**
- For DC series motor, the field current is equal to the armature current i.e.  $I_{field} = I_a$ .
- Hence in dc series motor, torque is proportional to the square of armature current.

#### • Speed Equations:

➤ We know that the expression for the back emf is,

▶ But P, Z and 60A ai E<sub>b</sub> ∝ ø N<sup>E</sup>b = MPφZ/60 A
Therefore we can write that, E<sub>b</sub> ∝ ø N<sup>E</sup>b = MPφZ/60 A
Therefore the speed can be expressed as, N ∝ E<sub>b</sub>/ø .....(5) N = k E<sub>b</sub>/ø .....(6)
▶ But V = E<sub>b</sub> + I<sub>a</sub> R<sub>a</sub> ∴ E<sub>b</sub> = V - I<sub>a</sub> R<sub>a</sub> .....(7)
▶ Substituting eq.(7) into eq.(5) we get, N ∝ (V - I<sub>a</sub> R<sub>a</sub>) / ø .....(8)
▶ Since ø ∝ I<sub>field</sub>, we can write, N ∝ (V - I<sub>a</sub> R<sub>a</sub>) / I<sub>field</sub> ......(9)

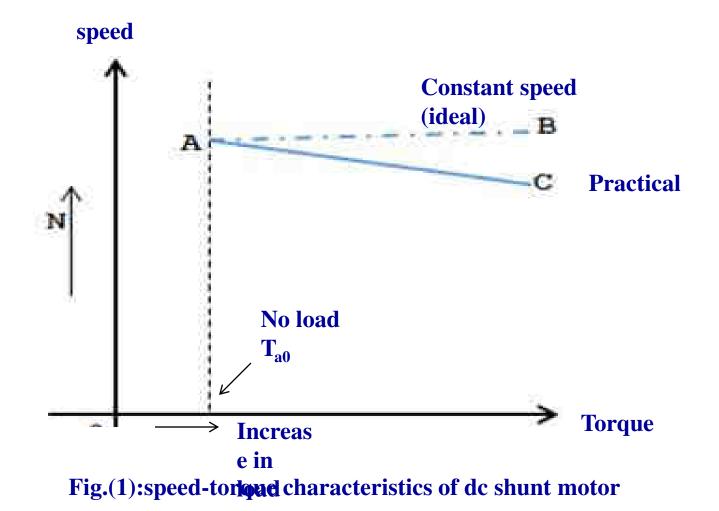
- 1. DC shunt motor:
- For dc shunt motor, the flux  $\phi$  is constant.  $\therefore N \propto (V - I_a R_a) \qquad \dots (10)$
- 2. DC series motor:
- ➢ For dc series motor I<sub>field</sub> = I<sub>a</sub>. Therefore
  N ∝ (V I<sub>a</sub> R<sub>a</sub> I<sub>s</sub> R<sub>s</sub>) / I<sub>a</sub> .....(11)
  where E<sub>b</sub> = V I<sub>a</sub> R<sub>a</sub> I<sub>s</sub> R<sub>s</sub>

### **Torque-speed characteristics**

### 1. DC shunt motor:

- The torque-speed characteristics of dc shunt motor is as shown in fig.(1).
- At no load, the torque produced by the motor is  $T_{a0}$  and the motor rotates at the no load speed  $N_0$ .
- As the load increased, the torque requirement also increase. To generate the required amount of torque, the motor has to draw more armature current.

- And more armature current can be drawn if the more speed decreases.
- Therefore, as the load increases, torque will also increase and the speed decreases.
- However the reduction in speed is not significant as the load is increased from no load to full load. Therefore practically the dc shunt motor is called as a constant speed motor.



#### 2. DC series motor:

- The speed –torque characteristics of DC series motor is as shown in fig.(2).
- We know that

 $N \propto 1/I_a$  and  $T \propto I_a^2$  $N \propto 1/\sqrt{T}$  and  $I_a \propto \sqrt{T}$ 

• This shows that the speed decreases with increase in the value of torque.

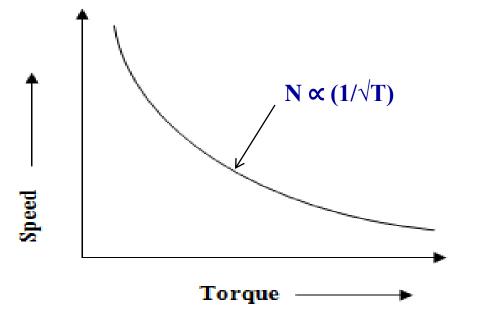
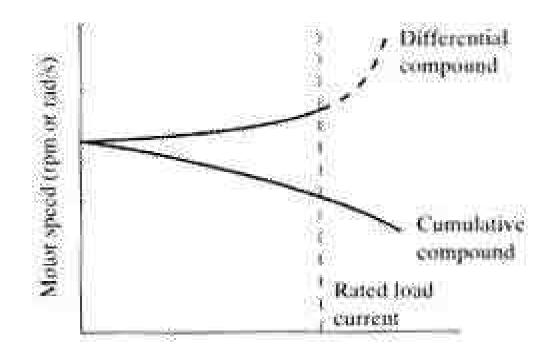


Fig.(2): speed-torque characteristics of dc series motor

#### 3. DC compound motor:

- The torque- speed characteristics of the DC compound motor is as shown in fig.(3).
- It is combination of characteristics of DC series and DC shunt motor.
- The exact shape of these characteristics is dependent on the precise effects of series and shunt field winding.



**Fig.(3): speed torque characteristics of dc compound motor** 

## **Applications of DC Motor**

- **1. Shunt motor applications:**
- i. Various machine tools such as lathe machines, drilling machines, milling machines etc.
- ii. Printing machines
- iii. Paper machines
- iv. Centrifugal and reciprocating pumps
- v. Blowers and fans etc.

### **2.** Series motor applications:

- i. Electric trains
- ii. Diesel-electric locomotives
- iii. Cranes
- iv. Hoists
- v. Trolley cars and trolley buses
- vi. Rapid transit systems
- vii. Conveyers etc.

#### 3. Cumulative compound motor applications:

- i. Elevators
- ii. Rolling mills
- iii. Planers
- iv. Punches
- v. Shears

#### 4. Differentials compound motors applications:

- ➢ The speed of these motors will increase with increase in the load, which leads to an unstable operation.
- Therefore we can not use this motor for any practical applications

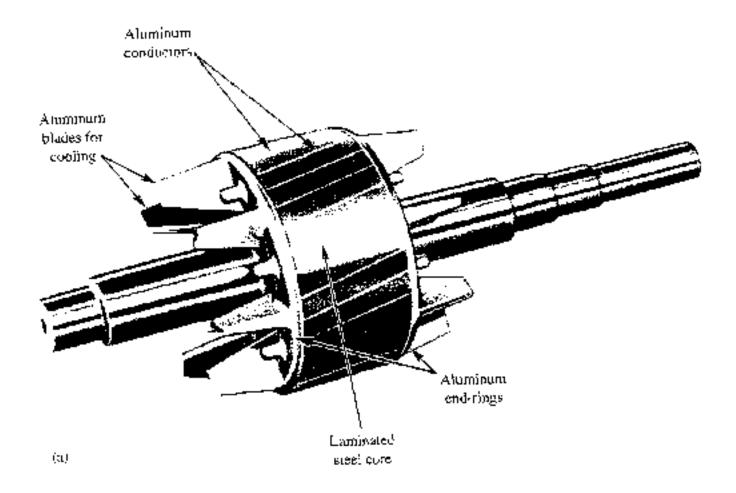
## **Specifications of DC Motor**

- Some of important specifications of a DC motor:
- 1. Output power in horse power(H.P.)
- 2. Rated voltage
- 3. Type of field winding
- 4. Excitation voltage
- 5. Base speed in RPM
- 6. Current
- 7. Frame size
- 8. Rating

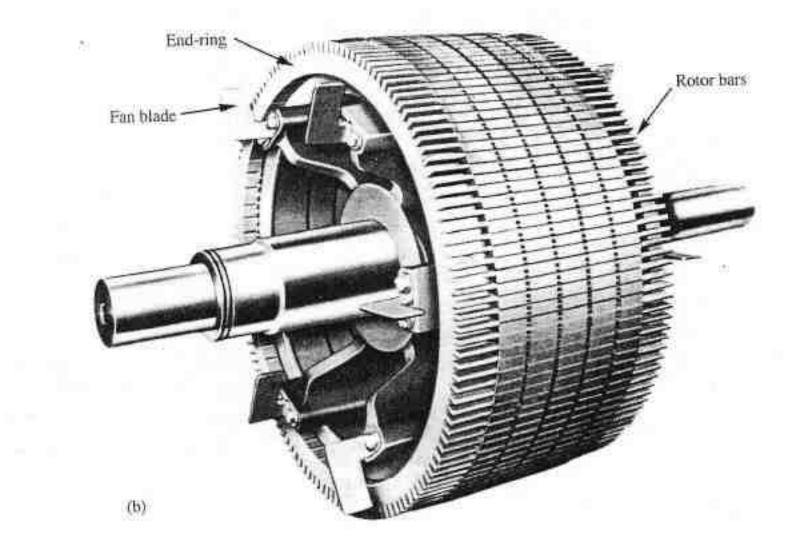
#### • Typical specifications of DC series motor:

Sr. No.	Specifications/Rating	Value
1.	Output power in horse power	3HP
2.	Rated voltage	230V
3.	Type of field winding	Series
4.	Excitation voltage	230V
5.	Insulation	В
6.	Base speed	1000RPM
7.	Current	11Amp
8.	Frame size	132 S
9.	Rating	Continous
10.	S.R.Number	840858

#### Squirrel-Cage Rotor

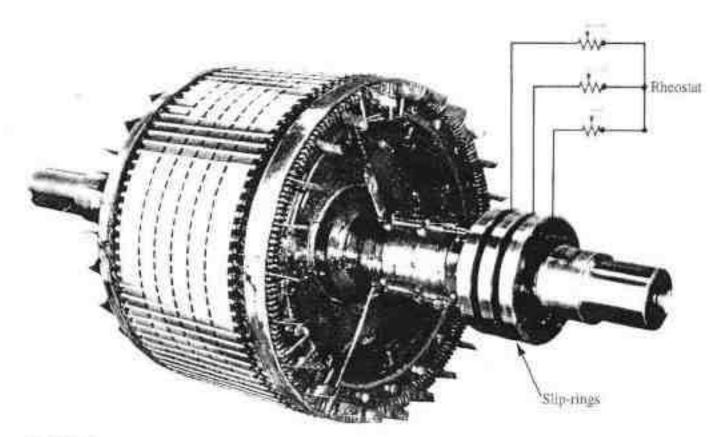


#### Another Squirrel-Cage Rotor



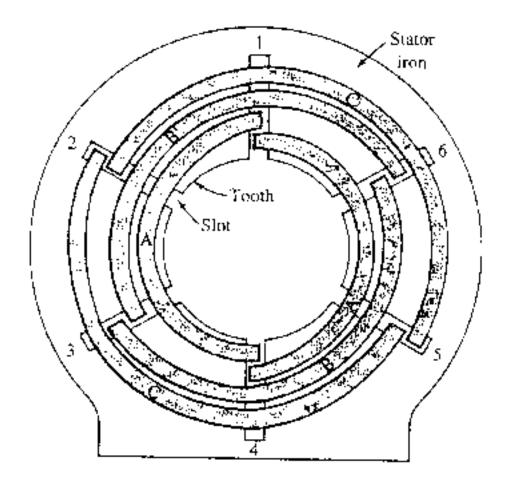
#### Wound-Rotor

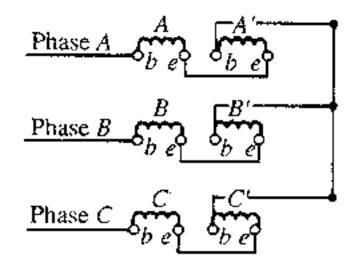
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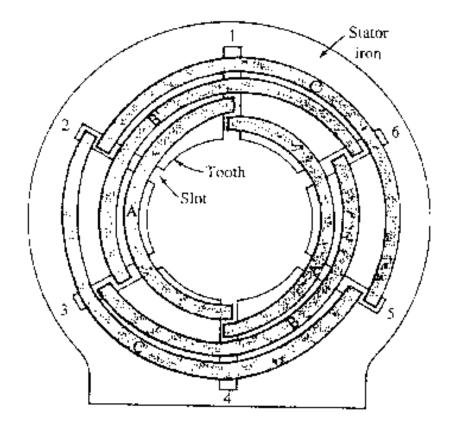
# Stator Coils for a 2-pole $3-\Phi$ induction motor

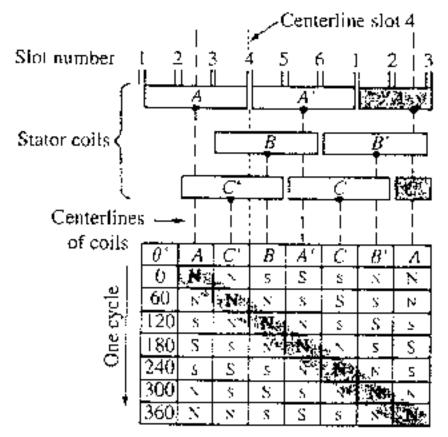




Connection diagram

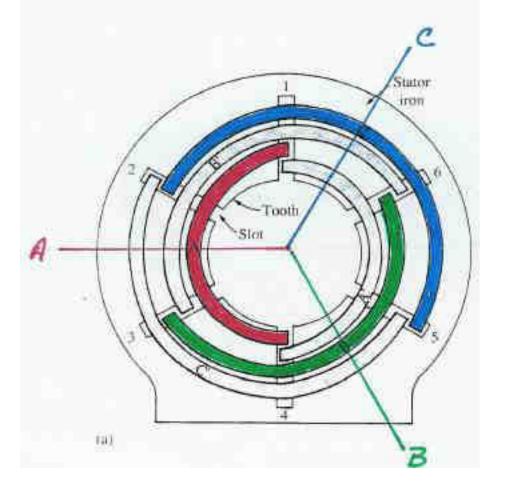
# Stator Coils for a 2-pole $3-\Phi$ induction motor





# Coil Span and distance between center lines

Coil Span = Stator circumference / # of stator poles Distance between center lines = 120°/ # of pole pairs



For a 2-pole machine,

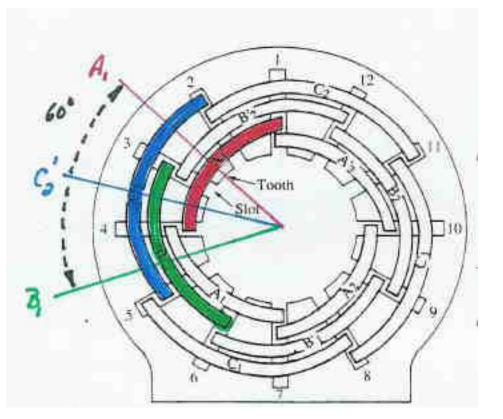
Coil Span = 360°/2 = 180°

**Center line distance = 120°** 

# Coil Span and distance between center lines

**Coil Span = Stator circumference / # of stator poles** 

**Distance between center lines = 120°/ # of pole pairs** 



For a 4-pole machine,

**Coil Span = 360°/4 = 90°** 

Center line distance = 60°

### Synchronous Speed

- n<sub>s</sub> = synchronous speed (r/min)
   the speed of the rotating magnetic flux
- $n_s = f_s/(P/2) (r/s)$ 
  - where
    - $f_s = frequency of the 3-\Phi$  supply
    - $n_s = synchronous speed$
    - P = number of poles formed by the stator winding
- $n_s = 120(f_s)/P$  (r/min)

## Slip

- $n_s =$  synchronous speed of the rotating flux
- $n_r$  = speed of the rotor
- slip speed =  $n = n_s n_r$
- slip = s =  $(n_s n_r) / n_s$  = per-unit slip
- % slip = s x 100%
- solving for  $n_r$ ,
- $n_r = n_s(1-s)$

### Effect of slip on rotor frequency

- frequency of the voltage induced in the rotor, f<sub>r</sub>
- $f_r = Pn/120$ , where
  - -P = the number of stator poles
  - -n =the slip speed (r/min)
  - $f_r = rotor frequency (Hz) = P(n_s n_r)/120$

 $-f_r = P(sn_s)/120 = s(Pn_s/120) = proportional to s!$ 

#### "Blocked rotor" condition (n<sub>r</sub>=0)

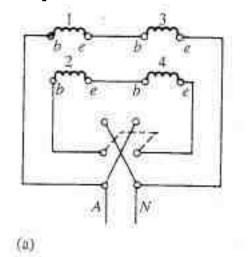
• 
$$s = (n_s - n_r)/n_s = (n_s - 0)/n_s = 1$$

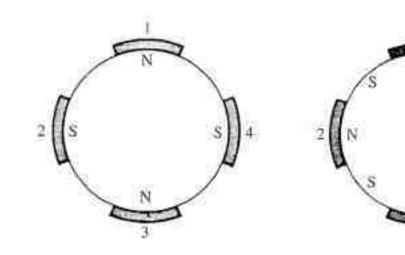
- $f_r = s(Pn_s/120) = Pn_s/120 = same as source$
- $f_r = f_{BR} = f_{stator}$
- In general,  $f_r = sf_{BR}$

#### Effect of slip on rotor voltage

- For a squirrel-cage rotor,  $->E_r = 4.44Nf_r\Phi_{max} = 4.44Nsf_{BR}\Phi_{max}$
- at blocked rotor, s=1  $->E_{BR} = 4.44Nf_{BR}\Phi_{max} =>E_r = sE_{BR}$

#### **Consequent-Pole Motor**

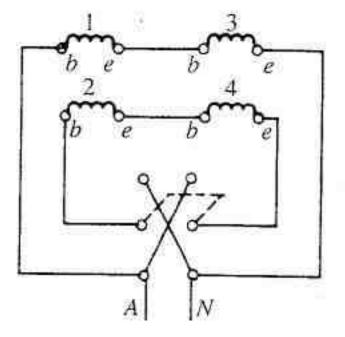




**4-pole machine** 

8-pole machine

### Winding Connections



Switch "up", coils 1 & 3 have opposite polarity to coils 2 & 4. Looks like a 4-pole machine. (Fast)

Switch "down", all coils have the same polarity. Looks like an 8-pole machine.

## SYNCHRONOUS GENERATORS Summary

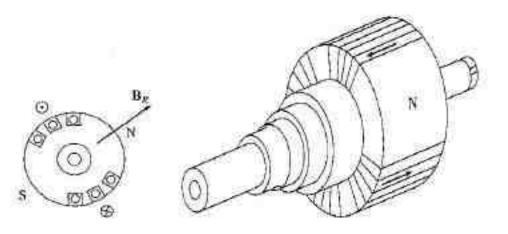
- 1. Synchronous Generator Construction
- 2. Speed of Rotation of a Synchronous Generator
- 3. Internal Voltage of a Synchronous Generator
- 4. Equivalent Circuit of a Synchronous Generator
- 5. Phasor Diagram of a Synchronous Generator Eq. cct.
- 6. Power and Torque in Synchronous Generator
- 7. Measuring Synchronous Generator Model Parameters

- SYN. GEN. USED to CONVERT MECHANICAL ENERGY TO AC ELECTRIC ENERGY: GENERATORS IN POWER PLANTS
- STEADY STATE OPERATION of SYNCHRONOUS GENERATORS DISCUSSED HERE

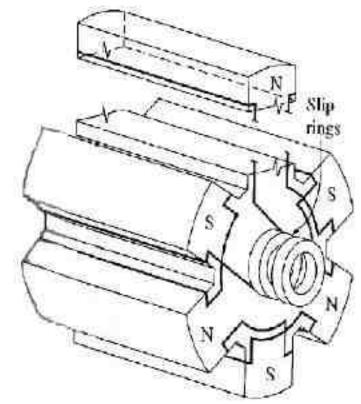
#### GENERATOR CONSTRUCTION

- in synchronous generator, rotor winding energized by dc source to develop rotor magnetic field
- rotor is turned by a prime mover, producing a rotating magnetic field which induce 3 phase voltages in stator windings
   In general rotor carry the "field windings", while "armature windings" (or "stator windings") carry the main voltages of machine
- therefore:
- rotor windings  $\equiv$  field windings
- stator windings ≡ armature windings

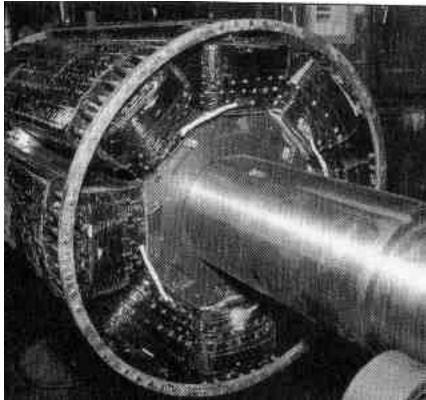
Rotor of synchronous machine can be
 Nonsalient: 2 pole rotor Salient: six-pole rotor



Side View



 Photograph of a salient 8-pole synchronous machine rotor



- Rotor experience varying magnetic fields, therefore is constructed of thin laminations to reduce eddy current losses
- To supply the rotor winding while it is rotating, special arrangement employed to connect its terminal to dc supply
  - supply dc power from an external dc source to rotor by means of slip rings
  - 2. supply dc power from a special dc power source mounted on shaft of rotor

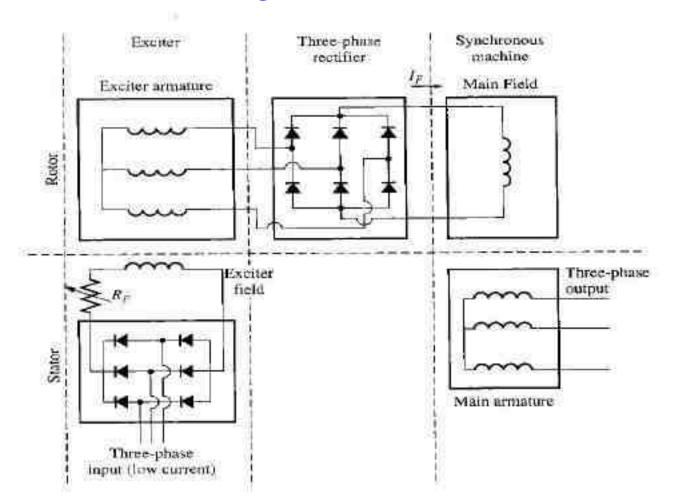
- SLIP RINGS: are metal rings encircling shaft and are insulated from it
  - one end of rotor winding is connected to each of the 2 slip rings
  - and a stationary brush mounted on the machine casing ride on each slip ring
- Brush: a block of graphite like carbon compound that conducts and has low friction
- same dc voltage is applied to field winding during rotation

- Problems associated with slip rings and brushes:
  - 1- increase the required maintenance (brushes should be examined for wear regularly)
  - 2- brush voltage drop results in significant power losses if field current is high
- Despite of above problems, SLIP RINGS & BRUSHES used for smaller synchronous machines since is cost-effective

- on larger generator & motors, brushless exciters are used
- Brushless Exciter: is a smaller ac generator with its field circuit mounted on stator & its armature circuit mounted on rotor shaft
  - 3 phase output of exciter generator rectified by
     a 3 phase rectifier mounted also on shaft
- By controlling small dc field current of exciter generator, it is possible to fed (and also adjust) field current of main machine without slip rings and brushes

## SYNCHRONOUS GENERATOR CONSTRUCTION

Schematic arrangement of a brushless exciter



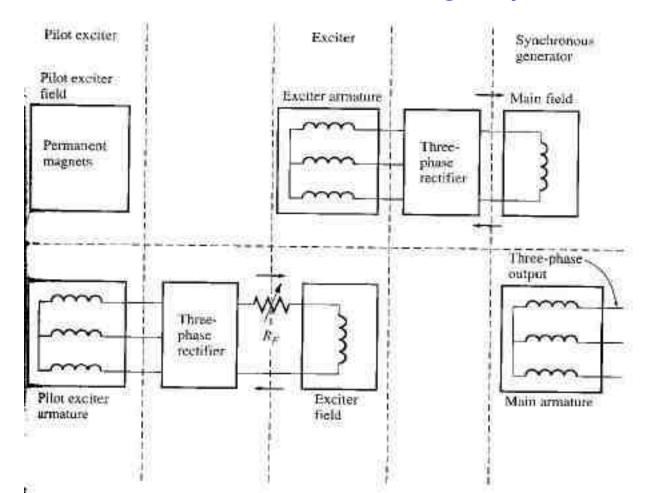
## SYNCHRONOUS GENERATOR CONSTRUCTION

 Photograph of a synchronous machine with brushless exciter

- a small pilot exciter often included in system to have the excitation of generator independent of any external power sources
- A pilot exciter is a small ac generator with permanent magnets mounted on rotor shaft & a 3 phase winding on stator
- It produces power for field circuit of exciter, which in turn controls the field circuit of main machine
- With pilot exciter on shaft of generator, no external electric power is required to run generator
- Many Syn. Gen.s with brushless exciters also have slip rings and brushes, as an auxiliary source of dc field in emergencies

# SYNCHRONOUS GENERATOR CONSTRUCTION

Brushless exciter including a pilot exciter



<u>SYNCHRONOUS GENERATOR</u> Speed of rotation of synchronous generator

- synchronous generators are *synchronous*, *during their operation*
- means: electrical frequency is synchronized with mechanical speed of rotor
- Relation between electrical frequency of stator and mechanical speed of rotor as shown before: f<sub>e</sub>=n<sub>m</sub> p / 120
  - fe: electrical frequency in Hz
  - nm: speed of rotor in r/min
  - p: number of poles

<u>SYNCHRONOUS GENERATOR</u> Speed of rotation of synchronous generator

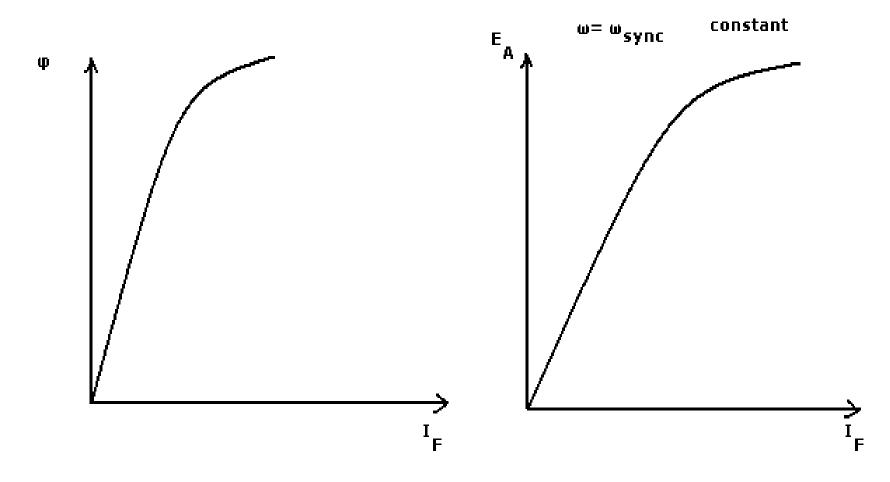
- Electric power generated at 50 or 60 Hz, so rotor must turn at fixed speed depending on number of poles on machine
- To generate 60 Hz in 2 pole machine, rotor must turn at 3600 r/min, and to generate 50 Hz in 4 pole machine, rotor must turn at 1500 r/min
- INTERNAL GENERATED VOLTAGE OF A SYNCHRONOUS GENERATOR
- magnitude of induced voltage in one phase determined in last section:  $E_A = \sqrt{2 \pi N_C \phi} f$

# <u>SYNCHRONOUS GENERATOR</u> INTERNAL GENERATED VOLTAGE

- Induced voltage depends on flux φ, frequency or speed of rotation f, & machine's construction
- Last equation can be rewritten as:  $E_A = K \phi \omega$   $K = Nc/\sqrt{2}$  (if  $\omega = \omega_e$ )
  - $K=Nc p/\sqrt{2} \qquad (if \omega = \omega_m)$
- Note: E<sub>A</sub> proportional to flux & speed, while flux depend on current in rotor winding I<sub>F</sub>, therefore E<sub>A</sub> is related to I<sub>F</sub> & its plot named: magnetization curve, or O/C characteristic

## <u>SYNCHRONOUS GENERATOR</u> INTERNAL GENERATED VOLTAGE

• Plots of flux vs IF and magnetization curve

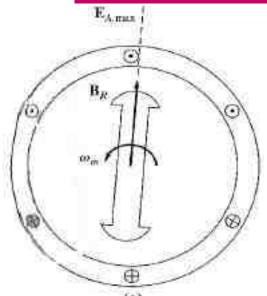


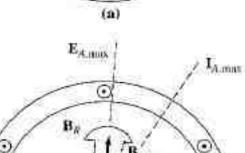
# <u>SYNCHRONOUS GENERATOR</u> <u>EQUIVALENT CIRCUIT</u>

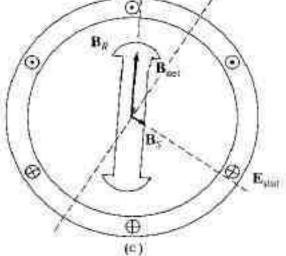
- To develop a relation for V<sub>φ</sub> as terminal voltage of generator which is different from internal voltage E<sub>A</sub> equivalent circuit is needed
- Reasons for  $V_{\phi}$  to be different from  $E_A$ 
  - 1- distortion of air-gap magnetic field magnetic field due to current flowing in stator, called *armature reaction*
- 2- self-inductance of armature coils
- 3- resistance of armature coils
- 4- effect of salient-pole rotor shapes (ignored as machines have cylindrical rotors)

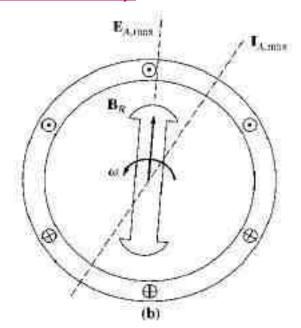
## SYNCHRONOUS GENERATOR

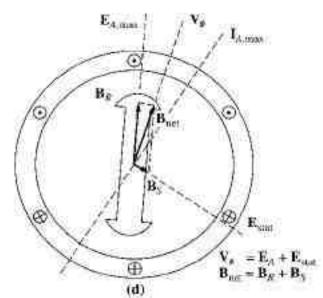
#### EQ. CCT. (ARM. REAC.)











<u>SYNCHRONOUS GENERATOR</u> <u>EQ. CCT. (ARM. REAC)...</u>

- Last figure shows a 2 pole rotor spinning inside a 3 phase stator, without load
- Rotor magnetic field B<sub>R</sub> develop a voltage E<sub>A</sub> as discussed in last chapter voltage is positive out of conductors, at top, and negative into the conductors at bottom of figure
- When there is no load on generator, armature current zero, E<sub>A</sub>=V<sub>φ</sub>
- If generator be connected to a lagging load, peak current occur at an angle behind peak voltage as in fig (b)

<u>SYNCHRONOUS GENERATOR</u> <u>EQ. CCT. (ARM. REAC)...</u>

- Current flowing in stator windings produces its magnetic field
- Stator magnetic field named Bs & its direction found by R.H.R. as shown in fig(c) this Bs produces another voltage in stator, named Estat and shown in figure
- Having these 2 voltage components in stator windings, total voltage in one phase is sum of EA and Estat :

V<sub>φ</sub>=E<sub>A</sub>+E<sub>stat</sub> and B<sub>net</sub>=B<sub>R</sub>+B<sub>S</sub>

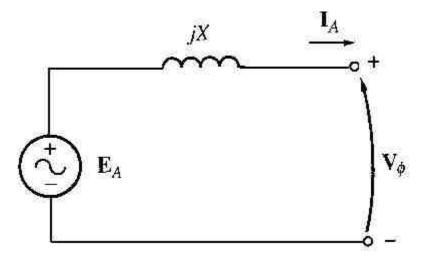
angle of  $B_{net}$  coincide with angle of  $V_{\phi}$  shown in fig (d)

## SYNCHRONOUS GENERATOR EQ. CCT. (ARM. REAC)...

- To model effect of armature reaction, note:
  - 1- Estat lies at an angle of 90° behind plane of maximum current IA
  - 2- Estat directly proportional to IA and X is constant of proportionality
- $\rightarrow$  voltage in one phase  $V_{\varphi} = E_{A-j} X I_{A}$

 $\rightarrow$ 

- Following eq. cct. can be developed



<u>SYNCHRONOUS GENERATOR</u> <u>EQ. CCT. (ARM. REAC)...</u>

- Armature reaction voltage can be modeled as an inductor in series with internal induced voltage
- In addition to armature reaction, stator coils have a self-inductance and a resistance
- stator self-inductance named L<sub>A</sub> (its reactance X<sub>A</sub>) and stator resistance is R<sub>A</sub> :

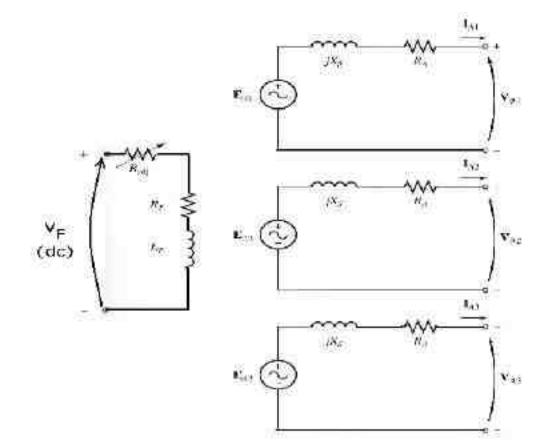
Vq=Ea- jXIa- jXaIa- RaIa

 Armature reaction & self-inductance in machine both represented by reactance, normally they are combined to a single reactance as : Xs=X+XA

V<sub>φ</sub>=Ea- jXs Ia- RaIa

### <u>SYNCHRONOUS GENERATOR</u> <u>EQ. CCT. (ARM. REAC)...</u>

 equivalent circuit of a 3 phase synchronous generator can be shown as follows:

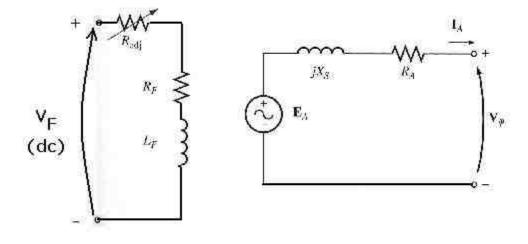


## SYNCHRONOUS GENERATOR EQ. CCT. ...

- Figure shows a dc source, supplying rotor winding, modeled by coil inductance & resistance in series with an adjustable resistor R<sub>adj</sub> that controls current
- Rest of equivalent circuit consists of model for each phase
- the voltages and currents of each phase are 120° apart with same magnitude
- Three phases can be connected in Y or  $\Delta$
- If connected in Y :  $V_T = \sqrt{3} V_{\phi}$
- If connected in  $\Delta$ :  $V_{T} = V_{\varphi}$

#### SYNCHRONOUS GENERATOR EQ. CCT...

• The per phase equivalent circuit is shown below



 can be employed when loads of 3 phase are balanced

# **Battery Overview**

Steve Garland Kyle Jamieson

# Outline

- Why is this important?
- Brief history of batteries
- Basic chemistry
- Battery types and characteristics
- Case study: ThinkPad battery technology

# Motivation

- To exploit properties of batteries in lowpower designs
  - Protocols (Span , MAC layer)
  - Hardware (Cricket)
  - Example: n cells; discharge from each cell, round-robin fashion [Chiasserini and Rao, INFOCOM 2000]

# Battery (Ancient) History

- 1800 Voltaic pile: silver zinc
- 1836 Daniell cell: copper zinc
- 1859 Planté: rechargeable lead-acid cell
- 1868 Leclanché: carbon zinc wet cell
- 1888 Gassner: carbon zinc dry cell
- 1898 Commercial flashlight, D cell
- 1899 Junger: nickel cadmium cell

# **Battery History**

- 1946 Neumann: sealed NiCd
- 1960s Alkaline, rechargeable NiCd
- 1970s Lithium, sealed lead acid
- 1990 Nickel metal hydride (NiMH)
- 1991 Lithium ion
- 1992 Rechargeable alkaline
- 1999 Lithium ion polymer

# **Battery Nomenclature**







**Duracell batteries** 

**9v battery** 

#### 6v dry cell

**Two cells** 

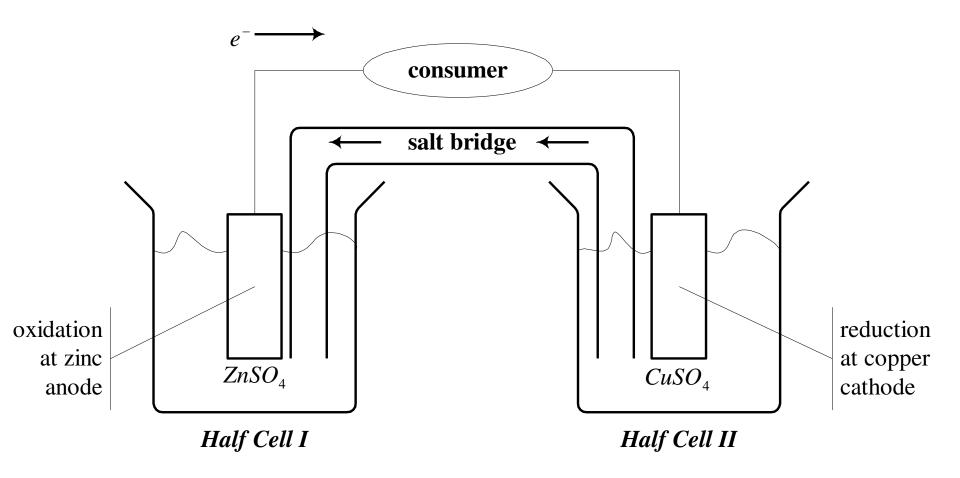
#### A real battery

**Another battery** 

**More precisely** 



# The Electrochemical Cell



# The Electrochemical Cell (2)

• Zinc is (much) more easily oxidized than Copper  $Zn \longrightarrow Zn^{2+} + 2e^{-}$  (*I*.)

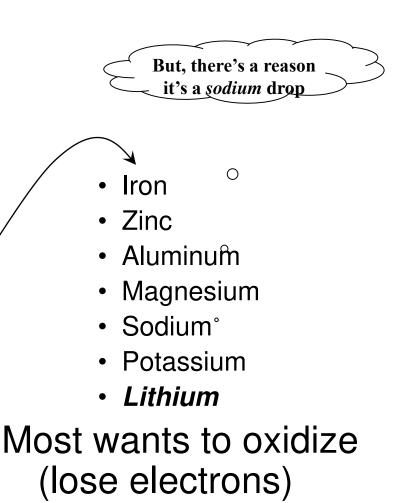
$$Cu^{2+} + 2e^{-} \longrightarrow Cu \quad (II.)$$

- Maintain equilibrium electron densities
  - Add copper ions in solution to Half Cell II
- Salt bridge only carries negative ions
  - This is the limiting factor for current flow
  - Pick a low-resistance bridge

# The Electrochemical Series

Most wants to reduce (gain electrons)

- Gold
- Mercury
- Silver
- Copper
- Lead
- Nickel
- Cadmium



# **Battery Characteristics**

- Size
  - Physical: button, AAA, AA, C, D, ...
  - Energy density (watts per kg or cm<sup>3</sup>)
- Longevity
  - Capacity (Ah, for drain of C/10 at  $20^{\circ}$ C)
  - Number of recharge cycles
- Discharge characteristics (voltage drop)

# **Further Characteristics**

- Cost
- Behavioral factors
  - Temperature range (storage, operation)
  - Self discharge
  - Memory effect
- Environmental factors
  - Leakage, gassing, toxicity
  - Shock resistance

# Primary (Disposable) Batteries

- Zinc carbon (flashlights, toys)
- Heavy duty zinc chloride (radios, recorders)
- Alkaline (all of the above)
- Lithium (photoflash)
- Silver, mercury oxide (hearing aid, watches)
- Zinc air

# Standard Zinc Carbon Batteries

• Chemistry

Zinc (-), manganese dioxide (+) Zinc, ammonium chloride aqueous electrolyte

- Features
  - + Inexpensive, widely available
  - Inefficient at high current drain
  - Poor discharge curve (sloping)
  - Poor performance at low temperatures

# Standard Alkaline Batteries

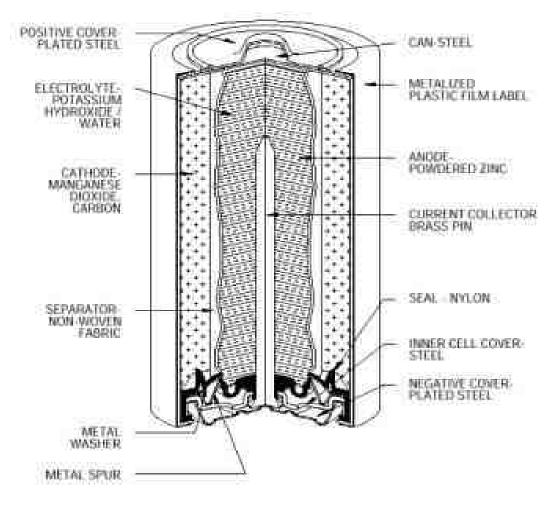
• Chemistry

Zinc (-), manganese dioxide (+) Potassium hydroxide aqueous electrolyte

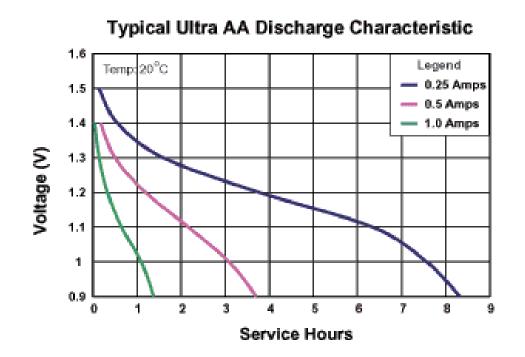
- Features
  - + 50-100% more energy than carbon zinc
  - + Low self-discharge (10 year shelf life)
  - ± Good for low current (< 400mA), long-life use
  - Poor discharge curve

# Alkaline-Manganese Batteries (2)

EVEREADY ENERGIZER ALKALINE "D" SIZE



# Alkaline Battery Discharge



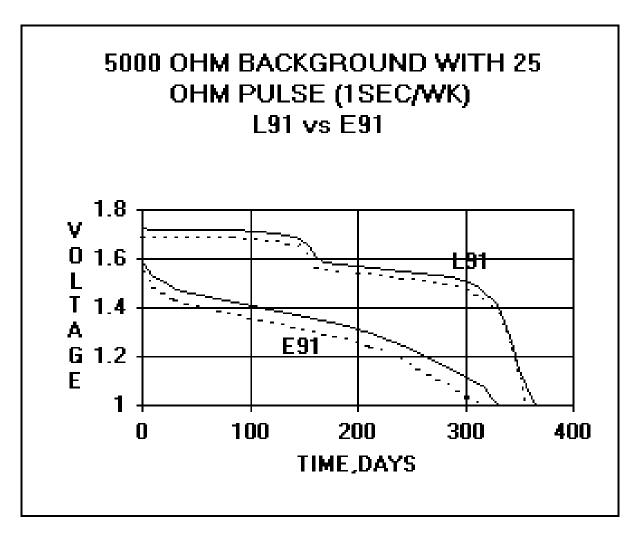
# Lithium Manganese Dioxide

• Chemistry

Lithium (-), manganese dioxide (+) Alkali metal salt in organic solvent electrolyte

- Features
  - + High energy density
  - + Long shelf life (20 years at 70°C)
  - + Capable of high rate discharge
  - Expensive

# Lithium v Alkaline Discharge



# Secondary (Rechargeable) Batteries

- Nickel cadmium
- Nickel metal hydride
- Alkaline
- Lithium ion
- Lithium ion polymer
- Lead acid

# Nickel Cadmium Batteries

• Chemistry

Cadmium (-), nickel hydroxide (+) Potassium hydroxide aqueous electrolyte

- Features
  - + Rugged, long life, economical
  - + Good high discharge rate (for power tools)
  - Relatively low energy density
  - Toxic

# NiCd Recharging

- Over 1000 cycles (if properly maintained)
- Fast, simple charge (even after long storage)

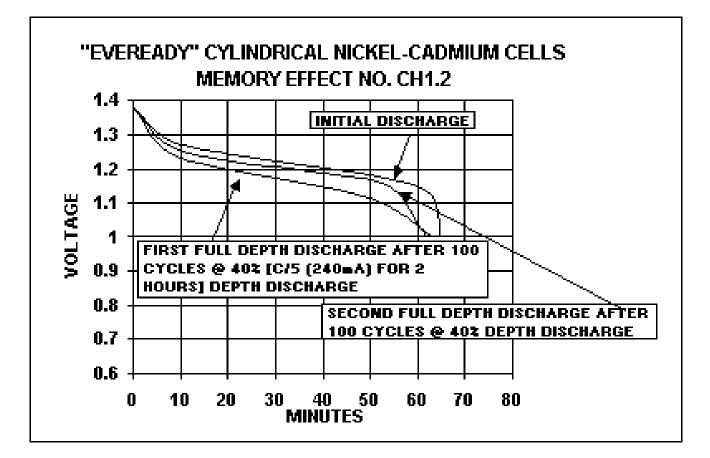
C/3 to 4C with temperature monitoring

- Self discharge

   10% in first day, then 10%/mo
   Trickle charge (C/16) will maintain charge
- Memory effect

Overcome by 60% discharges to 1.1V

# NiCd Memory Effect



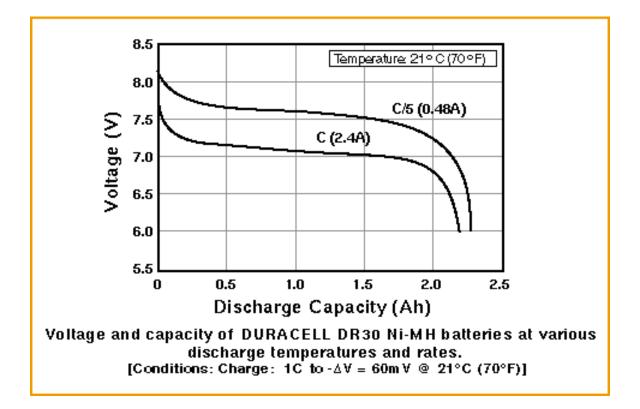
#### Nickel Metal Hydride Batteries

• Chemistry

LaNi<sub>5</sub>, TiMn<sub>2</sub>, ZrMn<sub>2</sub> (-), nickel hydroxide (+) Potassium hydroxide aqueous electrolyte

- Features
  - + Higher energy density (40%) than NiCd
  - + Nontoxic
  - Reduced life, discharge rate (0.2-0.5C)
  - More expensive (20%) than NiCd

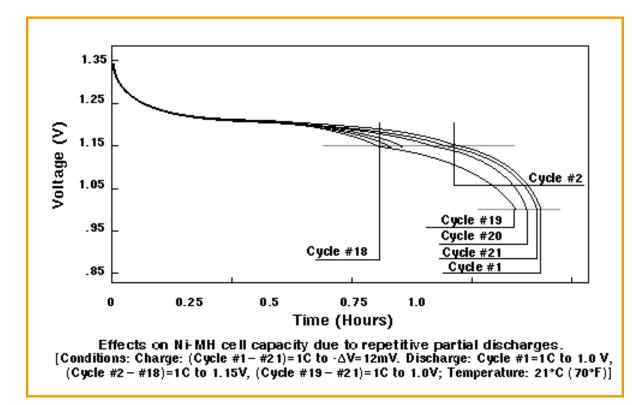
#### NiMH Battery Discharge



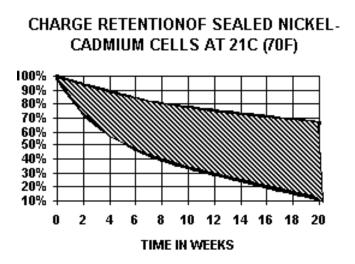
### NiMH Recharging

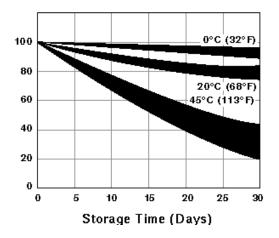
- Less prone to memory than NiCd
- Shallow discharge better than deep Degrades after 200-300 deep cycles Need regular full discharge to avoid crystals
- Self discharge 1.5-2.0 more than NiCd
- Longer charge time than for NiCd To avoid overheating

#### NiMH Memory Effect



#### NiCd v NiMH Self-Discharge

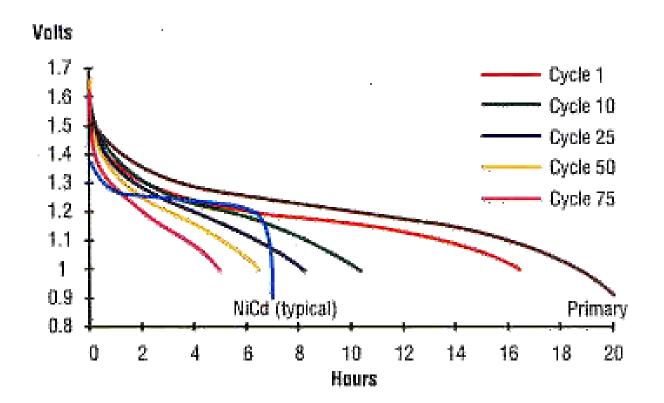




#### Secondary Alkaline Batteries

- Features
  - 50 cycles at 50% discharge
  - No memory effect
  - Shallow discharge better than deeper

#### NiCd v Alkaline Discharge



#### Lead Acid Batteries

- Chemistry
  - Lead
  - Sulfuric acid electrolyte
- Features
  - + Least expensive
  - + Durable
  - Low energy density
  - Toxic

#### Lead Acid Recharging

- Low self-discharge
  - 40% in one year (three months for NiCd)
- No memory
- Cannot be stored when discharged
- Limited number of full discharges
- Danger of overheating during charging

#### Lithium Ion Batteries

• Chemistry

Graphite (-), cobalt or manganese (+) Nonaqueous electrolyte

- Features
  - + 40% more capacity than NiCd
  - + Flat discharge (like NiCd)
  - + Self-discharge 50% less than NiCd
  - Expensive

#### Lithium Ion Recharging

- 300 cycles
- 50% capacity at 500 cycles

#### Lithium Ion Polymer Batteries

• Chemistry

Graphite (-), cobalt or manganese (+) Nonaqueous electrolyte

- Features
  - + Slim geometry, flexible shape, light weight
  - + Potentially lower cost (but currently expensive)
  - Lower energy density, fewer cycles than Liion

#### **Battery Capacity**

Туре	Capacity (mAh)	Density (Wh/kg)
Alkaline AA	2850	124
Rechargeable	1600	80
NiCd AA	750	41
NiMH AA	1100	51
Lithium ion	1200	100
Lead acid	2000	30

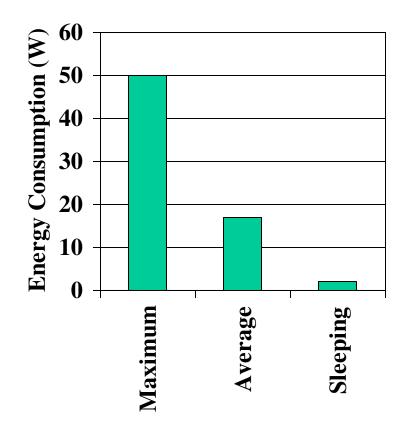
#### **Discharge Rates**

Туре	Voltage	Peak	Optimal
		Drain	Drain
Alkaline	1.5	0.5C	< 0.2C
NiCd	1.25	20C	1C
Nickel metal	1.25	5C	< 0.5C
Lead acid	2	5C	0.2C
Lithium ion	3.6	2C	< 1C

#### Recharging

Туре	Cycles (to 80%)	Charge time	Discharge per month	Cost per kWh
Alkaline	50 (50%)	3-10h	0.3%	\$95.00
NiCd	1500	1h	20%	\$7.50
NiMH	300-500	2-4h	30%	\$18.50
Li-ion	500-1000	2-4h	10%	\$24.00
Polymer	300-500	2-4h	10%	
Lead acid	200-2000	8-16h	5%	\$8.50

#### Example: IBM ThinkPad T21 Model 2647



- Source: IBM datasheet
- Relatively-constant discharge

## Lithium-ion Batteries in Notebooks

- Lithium: greatest electrochemical potential, lightest weight of all metals
  - But, Lithium metal is explosive
  - So, use Lithium-{cobalt, manganese, nickel} dioxide
- Overcharging would convert lithium-x dioxide to metallic lithium, with risk of explosion

#### IBM ThinkPad Backup Battery

- Panasonic CR2032 coin-type lithiummagnesium dioxide primary battery
  - Application: CMOS memory backup
  - Constant discharge, ~0.1 mA
  - Weight: 3.1g
  - 220 mA-h capacity



#### IBM ThinkPad T21 Main Battery

- Lithium-ion secondary battery
- 3.6 A-h capacity at 10.8V
- Back-of-the-envelope calculations from workload shown earlier:
  - Maximum: 47 minutes
  - Average: 2 hours, 17 minutes
  - Sleep: 19 hours?

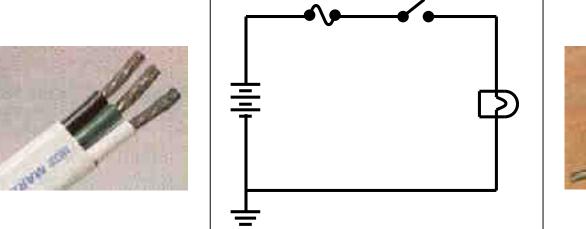
#### References

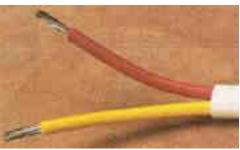
# Manufacturers www.duracell.com/OEM data.energizer.com www.rayovac.com/busoem/oem

- Books
  - T. R. Crompton, Battery Reference Book, Newnes, 2000
  - D. Berndt, Maintenance-Free Batteries, Wiley, 1997
  - C. Vincent & B. Scrosati, Modern Batteries, Wiley, 1997
  - I. Buchmann, *Batteries in a Portable World*, www.buchmann.ca

#### Chapter 2

## Electrical Wiring Practices and Diagrams





**MElec-Ch2 - 201** 

#### Overview

- Safety
- Standards
- Wiring Considerations
- Wire Terminations
- Coaxial Cable
- Wiring Installations
- Wiring Diagrams

#### Safety

Lethal Current

Safety Precautions

#### Lethal Current

- Fundamental policy of the USPS is SAFETY
- Human Body
  - Resistance 4 K $\Omega$  (moist skin) to 24 K $\Omega$  (dry skin)
  - Safe current (through chest) less than 20 milliamps
  - E = 120 VAC  $R = 4 K\Omega$  I = ?
  - -I = 30 milliamps -NOT SAFE
  - Don't want current through chest cavity (may be lethal)

## Safety Precautions

- Turn circuit off
  - Disconnect service cord
  - Disconnect negative battery cable
- If must work on live AC circuit
   Need 2<sup>nd</sup> safety person
- Remove metal jewelry
- Know your boat and its wiring
- Use outlet tester on AC outlets
- Use 3-wire extension cord from GFI outlet

#### Standards

- American Boat and Yacht Council (ABYC)
  - AC and DC Electrical Systems is E-11
  - Minimum standards
    - Construction
    - Repair
- Marine Dept. of Underwriters Laboratory
  - Test and certify commercial products
  - Safety, not function

#### Wiring Considerations

Conductors

• Wire Types

• Wire Size

• Wire Insulation

Wire Color Code

**MElec-Ch2 - 207** 

#### Conductors

- Connects power sources to power loads
- Characteristics
  - Safe
  - Dependable
  - Efficient (minimal voltage drop)
- Boat environment
  - Worse than either house or car
  - High humidity
  - Vibration
  - Corrosive conditions

**MElec-Ch2 - 208** 

#### Wire Types

- Marine Grade
  - Type 3 is recommended

Stranded copper
 Tinned is preferred

ANCOR MARINE GRADE 4 AWG (UL) BOAT CABLE GOOV 105°C DRY 759C WEI DUL RESISTANT RCSW2 E67078 LL22035 CSA TEW 105°C OR AWM I A/B 105°C 600Y FT1

#### Wire Size

- 3% voltage drop
  - Critical circuits (Nav lights)
  - Electronic Equipment
- 10% voltage drop
  - Cabin lights
  - Motorized Equipment
- Minimum size AWG # 16



- Inadvertent Resistors
  - Wire too small (min of #16 properly size using table)
  - Bad connections (or corroded connections)
    - Clean and tighten battery connectors
    - Tighten lug screws and inspect wire to lug connection
  - Why do wires get warm / hot?
    - Low resistance circuits pass high current  $(P = I^2 \times R)$
    - Wires can account for much of the overall Mesistance

#### Wire Size Comparison



#### #16 top to #10 bottom



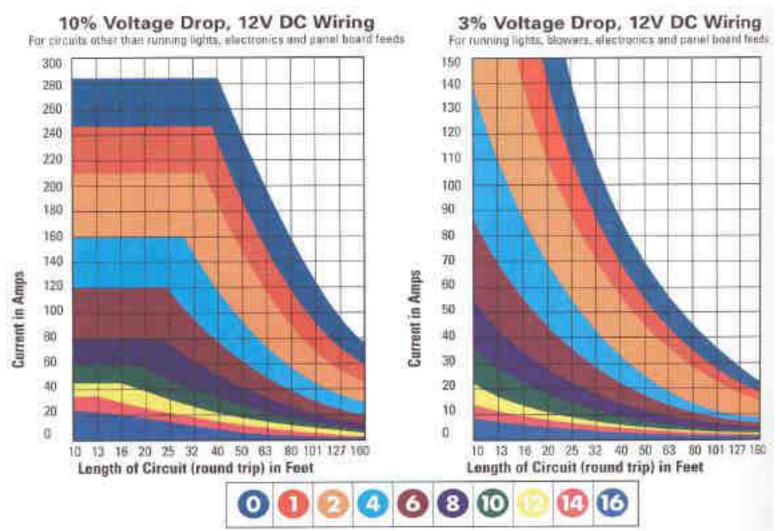
#### #2 top to #10 bottom

MElec-Ch2 - 212

#### **Copper Wire Characteristics**

American Wire Gauge #	NEC Ampacity TW insul.	Solid Wire Diameter in Mils	Nominal Cross Section Area in Circular Mils	Minimum # of Strands	Resistance Ohms per 1000 feet
18		40	1,620	16	6.39
16			2,580		4.02
14		64	4,110		2.53
12	.20	81	6,530	19	1.59
10	.30	102	10,380	19	1.00
8		129	16,510		0.628
6	55	162	26,240	37	0.395
4	70	204	41,740	61	0.249
3	85	229	52,640	61	0.197
2	95	258	66,360	127	0.1563
1	110	289	83,690	127	0.1239
0	125	325	105,600	127	0.0983
00		365	133,100	127	0.0779

#### 12- VDC Wire Size Selection



#### 12 VINC Wire Size Selection Table for 12 Volt Systems

Maximum length of run, in feet, of two-wire cable or dual conductors from battery terminals to equipment terminals.\*

Current					1	Vire Siz	e AWG	#				
Amperes	16	14	12	10	8	6	4	3	2	<b>1</b> {	0	0
5	8	14	24	38	61	96	_					
10	4	7	12	19	30	48	76					
15		4	8	13	20	32	- 51	- 64				
20	14		6	10	15	24	38	48	61			
30				6	10	16	25	32	. 41	51		
40	- 14	-	14	4	. 8	12	19	24	. 30	38	48	
55						9	14	18	22	-28	35	4
70	- 14	12			160		11	14	17	22	28	3
80				+				12	15	19		3
95	-			4	100		÷.		13	16	20	- 3
110	-								-	14	18	2
125			1.4		41		- X .	14			15	2
145			-	+							+	1

#### Wire Size Selection Table for Starter Motor Circuit Only

Maximum length of single wire, in feet, from battery positive terminal to main battery switch, to starter motor, to common negative bus, to battery negative terminal.

Current		50.45	1.1.2.5	a AWG#			245.5	070		
Amperes	12	10	8	6	4	3	2	1	0	00
150	- 22	- 54		- 4	10	13	16	20	26	32
200					8	10	12	15	19	- 24
250	×				. 6	8	10	12	15	19
300					5	6	8	10	13	16
400						5	6	8	10	12
500							.5	6	8	10
600			- 25		- 10			5	6	8
800									5	6
1.000				1.						5

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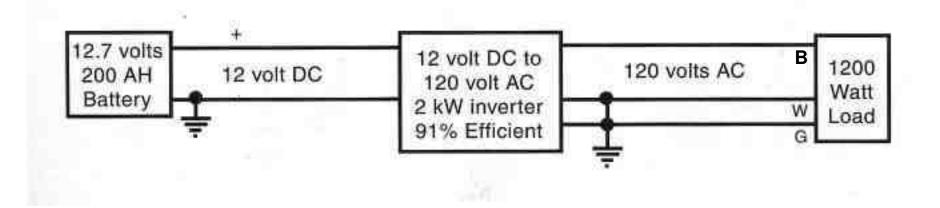
#### 120 VAC Wire Size Selection

Wire Size Selection Table for 120-Volt Systems

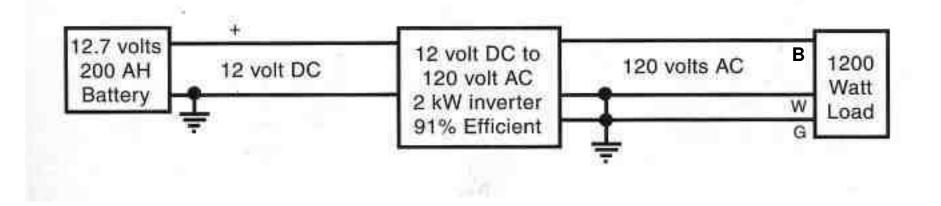
	CALL	Maximu	n length o						ctors			
Current	from power source to equipment terminals.* Wire Size AWG#											
Amperes	16	14	12	10	8	6	4	3	2	1	0	
5	88	142	226	360								
10	44	71	113	180		456						
15	and Vien	47	76	120		304	483					
20			57	90		228	362	457				
30	110× 01	116-31111	116 - 511	60		152	241	305	384			
40					72	114	181	228	288	363		
55	11	1108-000				83	132	166	209	264		
70				-	+		103	131	165	208	262	
80	ni 👻	n nae am	11- 111	0-00	W 40 - 1	1	- 14	114	144		229	
95	2	14			-		- 24	÷	121	153	193	
110		-		·····	23					132		
105		- 10 - 10 - 10 - 10 - 10 - 10 - 10 - 10	- MIL (1997)						· · · · · · · · · · · · · · · · · · ·	and the second	147	

\* Based on a Maximum Voltage Drop of 3% from source to load and a Supply Rating of 120 volts for American Wire Gauge Copper Conductors. If more current or a longer run is required, you must use a larger wire size to maintain the voltage drop at 3% or less.

## What Size Wires?



# Step 1



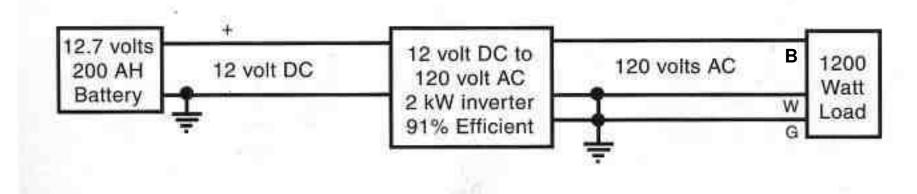
What current to Load? I = 10 Amps

P = E \* I I = P / E I = 1200/120

From Table 2-1 – For 10A need #16 wire

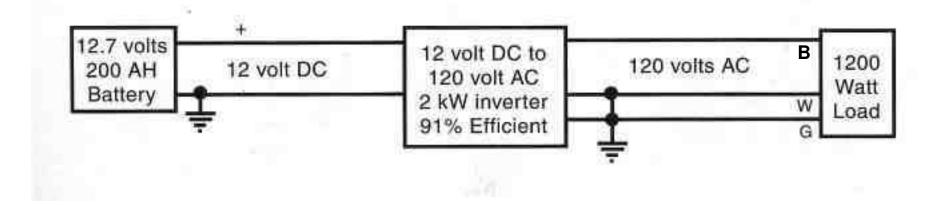
From Table 2-3 – Maximum of 44 feet (for 10A in #16 wire)

### Step 1 Answers AMPACITY 10 Amperes #16 AWG TW by Table 2-1



for 3% voltage drop 44 feet maximum by Table 2-3 MElec-Ch2 - 219

## Step 2



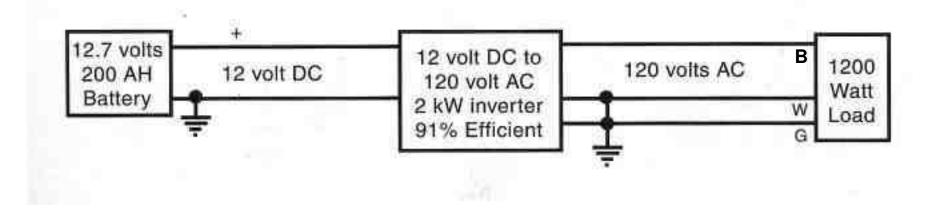
What current to Inverter?I<sub>load</sub> = 100 Amps @ 12 V

 $I_{load} = I_{out} = I_{in} *0.91$   $I_{in} = I_{out} / 0.91 = 100 / 0.91 = 110$  Amps

From Table 2-1 – For 110A need #1 wire

From Table 2-3 – Maximum of 14 feet (for 110A in #1 wire)





for 3% voltage drop 14 feet maximum by Table 2-2A

# Wire Insulation

- AC cables must be type UL 1426 BC
  - 600 volt insulation
  - Gasoline and Oil resistant
  - Won't absorb moisture
- DC wires & cables must be Marine Grade
  - 600 volt insulation
  - Gasoline and Oil resistant
  - Won't absorb moisture
- Color coded wires

## Wire Color Code

Color	AC (Hot)	AC (Neut) AC (Gnd)	DC +	DC -
Black	X			<b>X</b> <sup>1</sup>
White		X		
Green (m	nay have a <mark>y</mark>	ellow stripe) X		
Yellow				X1

Footnotes:

- 1 Yellow preferred for DC negative to avoid confusion with AC Hot wire
- $2 2^{nd}$  hot wire in 220 VAC is Red

### Wira Color Coding for DC and AC Wiring

Wire Color	DC Wiring*		
Black or Yellow	DC Negative Conductors		
Red	DC Positive Conductors		
Yellow with Red Stripe	Starter Switch to Solenoid		
Yellow	Bilge Blower (See note below)		
Brown with Yellow Stripe	Bilge Blower (See note below)		
Dark Gray	Navigation Lights, Tachometer Sensor to Indicator		
Brown	Pump Circuits and from (1) Generator Armature to Regulator,		
	or (2) Alternator Auxiliary Terminal to Regulator		
Orange	Distribution Panel to Accessory Switch; Ammeter to Alternator or Generator		
Purple	Ignition Switch to Coil & Instruments; Distribution Panel to Instruments		
Light Blue	Oil Pressure Sensor to Gauge		
Dark Blue	Cabin & Instrument Lights		
Pink	Fuel Level Sensor to Gauge		
Tan	Water Temperature Sensor to Gauge		
Green or Green with Yellow Stripe	Bonding (DC Grounding Conductors) wires only		
Green with Stripe	Deficient de la contra de la co		
(Any Stripe Color Stripe Except Vellow)	Tilt Down and/or Trim In		
Blue/Stripe	Tilt Up and/or Trim Out		
Note: If yellow is used for DC negative *DC Codes based on American Boat & Y	, blower must be brown with yellow stripe. (acht Council Recommendations.		

Wire Color	AC Wiring	
White	Current Carrying Neutral. Note: Can also be light blue	
Black	Hot Lead 120/240VAC Single Phase	
Red	2nd Hot Lead 120/240VAC Single Phase	
Green or Green with Yellow Stripe	Safety Grounding Conductor (AC)	
Bine	Additional Ungrounded Conductor (Usually Third Phase)	
Orange	Additional Ungrounded Conductor	12 - 224
	(Usually the High Leg on Center Grounded 240 VAC Delta Systems)	

# Wire Terminations

- Crimping
  - Special Tool
  - Approved Marine Connectors
  - Use of Ratcheting Tool
- Solder

Heat-shrink Tubing

## Wire Terminals



# Ratcheting Tool Use

- First select appropriate connector
- Strip insulation length of stem plus 1/16"
- Insert stripped end all way into terminal – End should extend 1/16"
- Place terminal in same color slot
  - First crimp end of terminal barrel nearest ring
  - Then crimp wire end of terminal barrel
- Check the connection with a solid tug

# Soldering

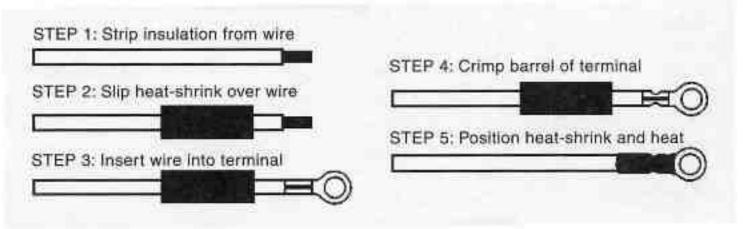
- Terminal connection can't be only soldered – Must also be crimped
- Soldering is normally not required

   Crimped connectors are acceptable to ABYC
   If solder, apply only to ring end of terminal
- Solder changes stranded wire into solid

   Stranded wire is flexible
- Use 40% lead / 60% tin, rosin core solder
- Battery lugs may be only soldered

## Heat-Shrink Tubing





### **Application Steps**

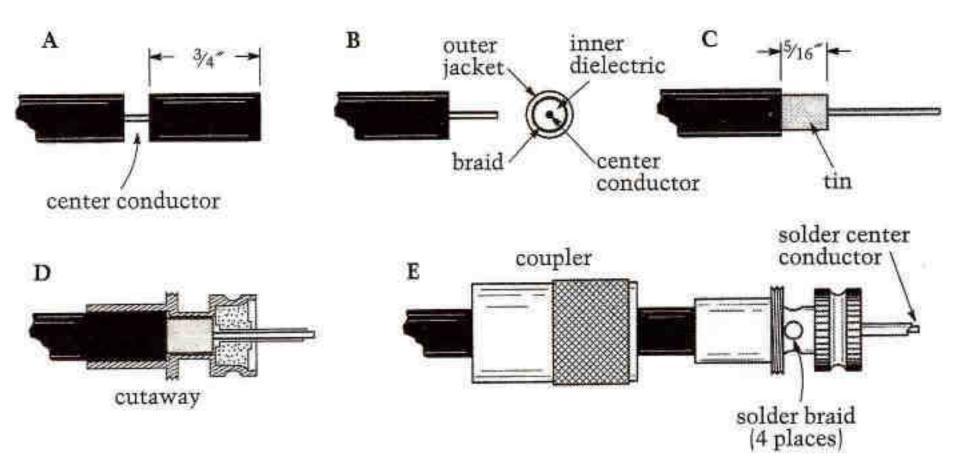
## **Coaxial Cable**

- Antenna cable
- Radio coax is 50 ohm with PL-259
- Radio cable is cut to length
- Want attenuation under 3 db
- TV cable is 75 ohm with "F" connectors
- GPS cable is not cut to length
   Coil excess in 1-foot loops

## **Coaxial Cable Information**

	impedance in Ohms	Attenuation @ 150 MHz	Outside Diameter	Bend Radius	Normal Connector	Remarks
Cable		per 100 ft		in inches		
RG-8/U	50	2.2	0.403	4	PL-259	
RG-BIX	50	3.2	0.242	2.4	PL-259	with adapter
RG-58A/U	50	5.8	0.194	2	PL-259	with adapter
RG-59/U	75	3.2	0.25	unk	Coaxial "F"	TV Coax
RG-213	50	3.2	0.405	5	PL-259	

## Soldering PL-259 Connector



# Wiring Installation

- Basic Considerations
- Distribution Panel
- Fuses / Circuit Breakers
- Branch Circuits
  - Wire
  - Outlets
  - Switches
- Grounding Systems
- Bonding Systems

## **Basic Considerations**

- Must have source and return wires
  - Return wires to a common point
  - May use feeder wire from power panel for:
    - engine, helm console, etc.
- Wires above flood level of bilge – Waterproof if in bilge
- Insulated support every 18"
- Twist DC wires within 1 meter of compass

## **Distribution Panel**

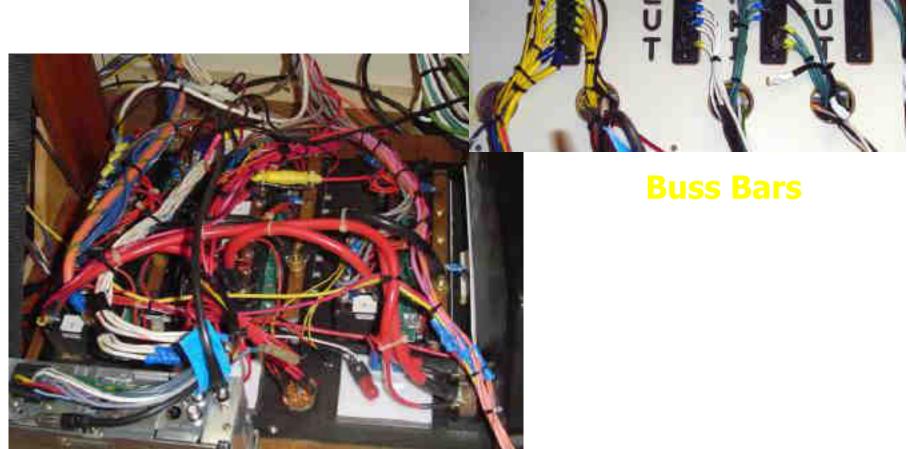
- Central location of Circuit Breakers / Fuses
   All branch circuits from this location
- AC and DC may be combined in one panel
- All equipment / circuits should go to panel – Not direct to battery (except bilge pump)
  - Noise interference suppression covered in Section 7

## DC / AC Power Panel



**Front View** 

### **Inside Power Panel**



**DC Side** 

## **Fuses and Circuit Breakers**

- Used to protect wiring from over current

   In positive or hot wire
- Newer boats use circuit breakers

   Initially more expensive
- Replace blown fuse with correct rating
- Circuit Breakers should be Marine Grade
  - Trip free
  - Manual reset



# **Branch Circuits - Wires**

- Minimum size is 16 AWG
  - See Wire Selection Tables
  - For AC normally #14 for 15A and #12 for 20A
- Must terminate in closed electrical box
- Of sufficient length
- DC negative returned to DC Panel

   May use several negative feeder terminals
- AC neutrals returned to AC Panel
- Bonding system never used as return wire

## Branch Circuits - Outlets

- 120 VAC outlets must be 3-wire polarized
   Black (hot) to brass or copper colored terminal
- Outlet wires must have crimp terminals
- GFI outlets
  - Required on weather deck, head, galley and machinery spaces
  - Good practice for all AC outlets to be GFI
  - Trip at 5 milliamps
- Different outlets for AC and DC power

## **Outlets and Plugs**

#### **12 VDC**



### **120 VAC**



### DC Outlet (Receptacle 15 A Outlet

#### **120 VAC**



#### **120 VAC**



#### GFI 15 A Outlet

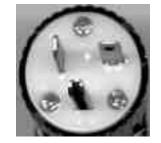
**20 A Outlet** 



**DC Plug** 







AC Plug 20 Elec-Ch2 - 241

## **Branch Circuits - Switches**

- Modern panels use Circuit Breakers

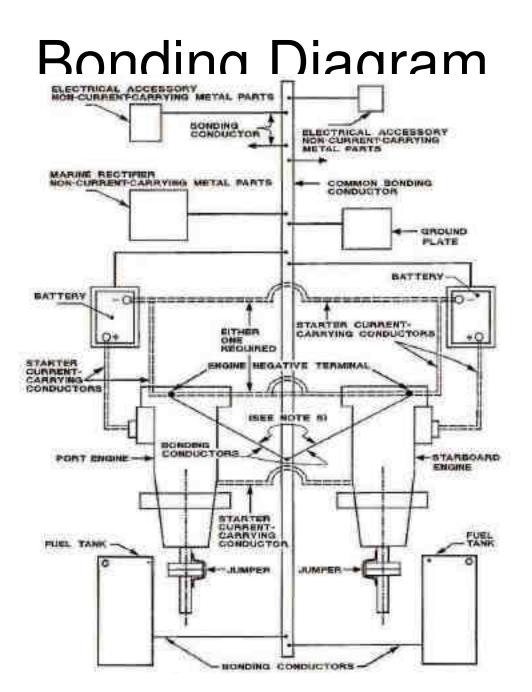
   Which also double as switches
- Switches / Circuit Breakers
  - Must be Marine Grade
  - Rated for the voltage and current controlled
  - Interrupt the positive (DC) or hot (AC) leg
- Battery Switch
  - Designed for high current service
  - Not located in engine or fuel-tank compartments

# Grounding System

- Ground is potential of water around boat
   Or potential of earth's surface
- DC Ground Battery negative terminal(s)
   Also engine block
   Wire color is Yellow (or Black)
- AC Transformer center tap on shore
  - Also connected to ground rod at transformer
  - Wire color is Green and uninterrupted wire
    - Isolation transformers and galvanic isolators are exception and covered in Chapter 4 on AC
- Engine, DC negative & AC ground connected

# Bonding System

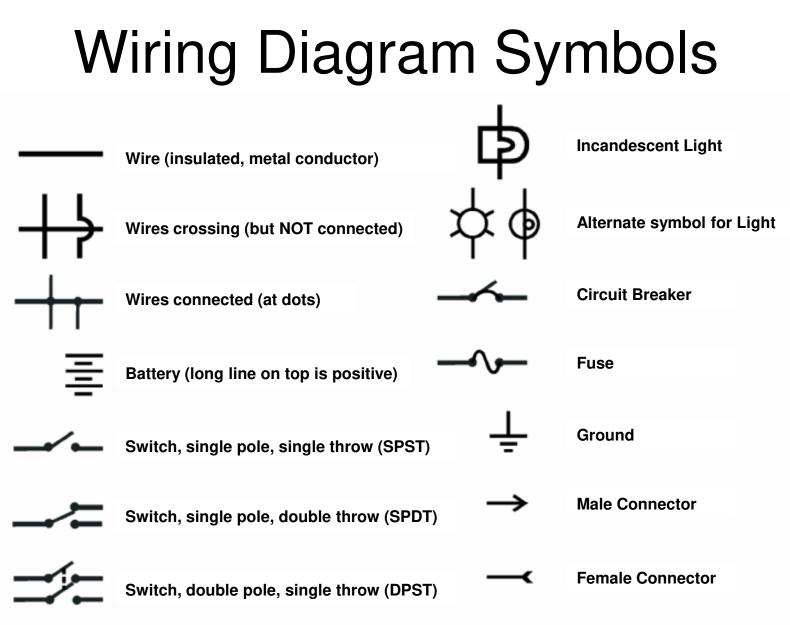
- For lightning protection
   More in Chapter 6
- All metal objects should be bonded
  - Keeps all metal at zero potential
  - Engine blocks
  - Battery negative terminals
- Non-current carrying wire
- Through-hull fittings
  - ABYC now recommends they be bonded
  - Electrically isolated from metal hullElec-Ch2 244



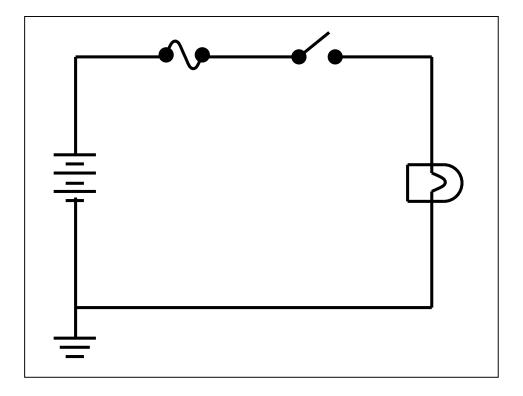
# Wiring Diagrams

- Elements of a Good Wiring Diagram
  - Documents boat's electrical layout
  - Should be kept current
  - Used for troubleshooting

- Component Identification
  - Physical objects to their symbol
  - Wires are color coded



## Simple DC Wiring Diagram



# Summary

- Circuits should be off when working on them
- Use only marine grade properly sized wires
  - Tables will help determine proper wire size
  - Minimum wire size is #16 AWG
- Use wire terminations and ratcheting crimper
- DC circuits are 2 dedicated wires
   Waterproof wire connection in bilge
- AC circuits are 3 dedicated wires

   GFCI in galley, head, machine spaces & weather deck
- Separate Grounding & Bonding systems required
   MElec-Ch2 249

• Keep wiring diagram current